# SUPPLEMENTARY INFORMATION

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# A Model governing equations

The model used throughout this work is a simple box model, a diagram of which can be seen in Supplementary Figure 1, and a summary of notation in Supplementary Table 6. There are two main stages: First the planetary embryos form, and differentiate into a metal core and a silicate mantle. It is assumed that the metal is in chemical equilibrium with the silicate as the embryo differentiates. The second stage comprises the accretion of the Earth from the planetary embryos. The mantle of the planetary embryos directly joins the mantle of the accreting Earth. The core of the planetary embryos takes two different routes to the core of the accreting Earth: A mass fraction k of the incoming core material equilibrates with the Earth's silicate mantle as it travels to the Earth's core, whereas a mass fraction 1-k is added directly to the Earth's core without any equilibration.

### A.1 Stable species

Consider first the case of stable species, such as a stable isotope or a trace element. The concentrations of a stable species in the mantle and core of the embryo are given by the usual equilibrium partitioning equations, namely

$$Fc_{ce} + (1 - F)c_{me} = c_{b}, \qquad \frac{c_{ce}}{c_{me}} = D_{c}$$
 (A.1)

or

$$c_{\text{me}} = \frac{c_{\text{b}}}{FD_c + (1 - F)}, \qquad c_{\text{ce}} = \frac{D_c c_{\text{b}}}{FD_c + (1 - F)},$$
 (A.2)

where  $c_{\text{me}}$  refers to the concentration in the mantle of the embryo,  $c_{\text{ce}}$  to the concentration in the core of the embryo, and  $c_{\text{b}}$  to the bulk concentration. F represents the mass fraction of metal, which will be assumed to be the same as the Earth's current core mass fraction, F = 0.323.  $D_c$  is the metal/silicate partition coefficient for the element in question. In general  $D_c$  is a function of the temperature, pressure, and oxygen fugacity conditions under which the metal/silicate equilibration takes place. As a simplifying assumption it will be assumed that all embryo material formed at the same temperature, pressure and oxygen fugacity conditions and thus  $D_c$  takes a single value for all embryo material.

The Earth accreted over a period of time, which will be represented by a function M(t) which determines the fraction of the Earth that has accreted at time t, where t=0 represents the beginning of accretion. Thus M(0)=0, and M(t)=1 when accretion has ceased. The entire mass of each embryo is assumed to join the mass of the Earth: we do not model "hit-and-run" collisions  $^{31,32}$ , where only part of the embryo material joins the Earth.

Conservation of mass in the accreting Earth can be described by the following equations for the Earth's mantle and core reservoirs

$$\frac{d}{dt} ((1 - F)Mc_{\rm m}) = [(1 - F)c_{\rm me} + kF(c_{\rm ce} - D_c c_{\rm m})] \frac{dM}{dt}, \tag{A.3}$$

$$\frac{\mathrm{d}}{\mathrm{d}t} (FMc_{\mathrm{c}}) = [kFD_{c}c_{\mathrm{m}} + (1-k)Fc_{\mathrm{ce}}] \frac{\mathrm{d}M}{\mathrm{d}t}, \tag{A.4}$$

where  $c_{\rm m}$  is the concentration of the chemical species in the Earth's mantle, and  $c_{\rm c}$  is the concentration in the Earth's core. A mass fraction F of the Earth is core, and 1 - F is mantle. Thus the quantities  $(1-F)Mc_{\rm m}$  and  $FMc_{\rm c}$  represent the relative number of moles of the chemical species in the two reservoirs. The two terms on the right hand side of (A.4) represent the two paths that metal from the embryos takes to the Earth's core:  $(1-k)Fc_{ce}$ represents the mass fraction 1-k which travels to directly to the core without reequilibration and thus records the embryo concentration, whereas  $kFD_cc_{\rm m}$  represents the mass fraction k which equilibrates with the mantle and thus has a composition in equilibrium with the Earth's mantle. The first term on the right hand side of (A.3),  $(1-F)c_{\text{me}}$ , represents the mantle embryo material that is added directly to the Earth's mantle, whereas  $kF(c_{ce}-D_cc_{m})$ represents the change in the Earth's mantle composition due to reequilibration with some of the incoming embryo core material. In general the partition coefficient  $D_c$  will be a function of time, since the pressure, temperature, and oxygen fugacity conditions under which metalsilicate equilibration occurred is expected to have changed as the Earth accreted. Note that the bulk concentration of the two reservoirs combined,  $Fc_c + (1 - F)c_m = c_b$  remains constant during the accretion, as can be seen by adding (A.3) and (A.4).

(A.3) and (A.4) can be rewritten as evolution equations for the concentrations  $c_{\rm m}$  and  $c_{\rm c}$ ,

$$\frac{\mathrm{d}c_{\mathrm{m}}}{\mathrm{d}t} = \left[c_{\mathrm{me}} + \frac{kF}{1 - F}c_{\mathrm{ce}} - \left(1 + \frac{kD_{c}F}{1 - F}\right)c_{\mathrm{m}}\right] \frac{1}{M} \frac{\mathrm{d}M}{\mathrm{d}t},\tag{A.5}$$

$$\frac{\mathrm{d}c_{\mathrm{c}}}{\mathrm{d}t} = \left[kD_{c}c_{\mathrm{m}} + (1-k)c_{\mathrm{ce}} - c_{\mathrm{c}}\right] \frac{1}{M} \frac{\mathrm{d}M}{\mathrm{d}t}.$$
(A.6)

There is a singularity in the above equation at t = 0 as a result of the initial zero mass fraction accreted, M(0) = 0. This singularity is removed by imposing the initial conditions  $c_{\rm m} = c_{\rm m0}$  and  $c_{\rm c} = c_{\rm c0}$  where

$$c_{\rm m0} = \frac{c_{\rm me} + kFc_{\rm ce}/(1-F)}{1 + kFD_c(0)/(1-F)},\tag{A.7}$$

$$c_{c0} = \frac{kD_c(0)c_{\text{me}} + ((1-k+kD_c(0)F/(1-F))c_{\text{ce}}}{1+kFD_c(0)/(1-F)},$$
(A.8)

where  $D_c(0)$  is the metal/silicate partition coefficient at time 0. The terms in square brackets in (A.5) and (A.6) are then initially zero and the singularity is removed. Starting from these initial conditions, (A.5) and (A.6) may be integrated to obtain the concentrations in the Earth's mantle and core.

### A.2 Parent isotope

Suppose a parent isotope p decays to a daughter isotope d with some decay constant  $\lambda$ . For simplicity, we will assume the embryos form at time 0 in the model. The initial concentrations of the parent isotope p in the embryos are given by equilibrium partitioning,

$$p_{\text{me0}} = \frac{p_{\text{b0}}}{FD_p + (1 - F)}, \qquad p_{\text{ce0}} = \frac{D_p p_{\text{b0}}}{FD_p + (1 - F)},$$
 (A.9)

where  $p_{b0}$  is the initial bulk concentration. The subsequent evolution in time is given by the usual radioactive decay law

$$p_{\text{me}} = p_{\text{me0}} e^{-\lambda t}, \qquad p_{\text{ce}} = p_{\text{ce0}} e^{-\lambda t}, \qquad p_{\text{b}} = p_{\text{b0}} e^{-\lambda t}.$$
 (A.10)

The concentration of the parent isotope in the Earth's mantle satisfies

$$\frac{\mathrm{d}p_{\mathrm{m}}}{\mathrm{d}t} = \left[ p_{\mathrm{me}} + \frac{kF}{1-F} p_{\mathrm{ce}} - \left( 1 + \frac{kD_{p}F}{1-F} \right) p_{\mathrm{m}} \right] \frac{1}{M} \frac{\mathrm{d}M}{\mathrm{d}t} - \lambda p_{\mathrm{m}}, \tag{A.11}$$

with initial condition

$$p_{\rm m0} = \frac{(1-F)p_{\rm me0} + kFp_{\rm ce0}}{1-F + kFD_p(0)}.$$
 (A.12)

Similar equations can be written for the Earth's core.

### A.3 Daughter isotope

The initial concentrations of the daughter isotope in the embryo are given by equilibrium partitioning as

$$d_{\text{me0}} = \frac{d_{\text{b0}}}{FD_d + (1 - F)}, \qquad d_{\text{ce0}} = \frac{D_d d_{\text{b0}}}{FD_d + (1 - F)}, \tag{A.13}$$

with subsequent evolution due to radioactive decay given by

$$d_{\text{me}} = d_{\text{me0}} + p_{\text{me0}} (1 - e^{-\lambda t}), \tag{A.14}$$

$$d_{\rm ce} = d_{\rm ce0} + p_{\rm ce0}(1 - e^{-\lambda t}),$$
 (A.15)

$$d_{\rm b} = d_{\rm b0} + p_{\rm b0}(1 - e^{-\lambda t}). \tag{A.16}$$

The concentration of the daughter isotope in the Earth's mantle satisfies

$$\frac{\mathrm{d}d_{\mathrm{m}}}{\mathrm{d}t} = \left[ d_{\mathrm{me}} + \frac{kF}{1-F} d_{\mathrm{ce}} - \left( 1 + \frac{kD_{d}F}{1-F} \right) d_{\mathrm{m}} \right] \frac{1}{M} \frac{\mathrm{d}M}{\mathrm{d}t} + \lambda p_{\mathrm{m}},\tag{A.17}$$

with initial condition

$$d_{\rm m0} = \frac{(1-F)d_{\rm me0} + kFd_{\rm ce0}}{1-F + kFD_d(0)}.$$
 (A.18)

# B Analytical solutions for constant partition coefficients

When the partition coefficients vary in time due to changing temperature, pressure, and oxygen fugacity conditions, the differential equations must be solved numerically. However, it is useful to examine the case of constant partition coefficients, where some analytical solutions are possible. Constant partitioning is assumed in Figures 2, 3, and 4. For the case of full equilibration (k = 1), the analytical solutions have been reviewed in detail by Jacobsen<sup>1</sup>. Here we generalise these solutions to the case of partial equilibration for some constant k, 0 < k < 1.

### B.1 Stable species

We will assume the same constant partition coefficient for both metal/silicate partitioning in the embryos and on Earth. It is convenient to introduce a new variable  $R_c = D_c F/(1 - F)$ . The embryo concentration in (A.2) can then be rewritten as

$$c_{\text{me}} = \frac{1}{1 + R_c} \cdot \frac{c_{\text{b}}}{1 - F}, \qquad c_{\text{ce}} = \frac{R_c}{1 + R_c} \cdot \frac{c_{\text{b}}}{F},$$
 (B.1)

and the initial Earth's mantle concentration from (A.7) is

$$c_{\text{m0}} = \frac{1}{1 + kR_c} \left( c_{\text{me}} + \frac{kF}{1 - F} c_{\text{ce}} \right) = \frac{1}{1 + R_c} \cdot \frac{c_{\text{b}}}{1 - F} = c_{\text{me}}.$$
 (B.2)

The mantle evolution equation from (A.5) is

$$\frac{\mathrm{d}c_{\mathrm{m}}}{\mathrm{d}t} = (1 + kR_c)\left(c_{\mathrm{m}0} - c_{\mathrm{m}}\right) \frac{1}{M} \frac{\mathrm{d}M}{\mathrm{d}t}$$
(B.3)

with initial condition  $c_{\rm m}=c_{\rm m0}$ . The solution of the above is simply that  $c_{\rm m}$  is constant,  $c_{\rm m}=c_{\rm m0}$  for all time. Thus the concentration is the same in the mantle of the embryos as in the mantle of Earth, and remains constant, as one would expect for the assumed constant partitioning behaviour.

### **B.2** Parent isotope

The concentrations of the parent isotope in the embryo are from (A.9) and (A.10)

$$p_{\text{me}} = \frac{1}{1 + R_p} \cdot \frac{p_{\text{b0}}}{1 - F} e^{-\lambda t}, \qquad p_{\text{ce}} = \frac{R_p}{1 + R_p} \cdot \frac{p_{\text{b0}}}{F} e^{-\lambda t},$$
 (B.4)

and the initial mantle concentration from (A.12) is

$$p_{\text{m0}} = \frac{1}{1 + kR_p} \left( p_{\text{me0}} + \frac{kF}{1 - F} p_{\text{ce0}} \right) = \frac{1}{1 + R_p} \cdot \frac{p_{\text{b0}}}{1 - F} = p_{\text{me0}}.$$
 (B.5)

The mantle evolution from (A.11) is

$$\frac{\mathrm{d}p_{\mathrm{m}}}{\mathrm{d}t} = (1 + kR_p) \left( p_{\mathrm{m}0} \mathrm{e}^{-\lambda t} - p_{\mathrm{m}} \right) \frac{1}{M} \frac{\mathrm{d}M}{\mathrm{d}t} - \lambda p_{\mathrm{m}}$$
 (B.6)

with initial condition  $p_{\rm m}=p_{\rm m0}$ . The solution of the above is simply  $p_{\rm m}=p_{\rm m0}{\rm e}^{-\lambda t}$ .

#### B.3 Daughter isotope

The concentrations of the daughter isotope in the embryo are from (A.13), (A.14), and (A.15)

$$d_{\text{me}} = \frac{1}{1 + R_d} \cdot \frac{d_{\text{b0}}}{1 - F} + \frac{1}{1 + R_p} \cdot \frac{p_{\text{b0}}}{1 - F} \left( 1 - e^{-\lambda t} \right), \tag{B.7}$$

$$d_{ce} = \frac{R_d}{1 + R_d} \cdot \frac{d_{b0}}{F} + \frac{R_p}{1 + R_p} \cdot \frac{p_{b0}}{F} \left( 1 - e^{-\lambda t} \right).$$
 (B.8)

Now, noting that

$$d_{\text{me}} + \frac{kF}{1 - F} d_{\text{ce}} = \frac{1 + kR_d}{1 + R_d} \frac{d_{b0}}{1 - F} + \frac{1 + kR_p}{1 + R_p} \frac{p_{b0}}{1 - F} \left( 1 - e^{-\lambda t} \right)$$
$$= (1 + kR_d) d_{m0} + (1 + kR_p) p_{m0} \left( 1 - e^{-\lambda t} \right), \tag{B.9}$$

the evolution of the daughter isotope in the mantle (A.17) may be written as

$$\frac{dd_{\rm m}}{dt} = \left[ (1 + kR_d) (d_{m0} - d_{\rm m}) + (1 + kR_p) p_{m0} \left( 1 - e^{-\lambda t} \right) \right] \frac{1}{M} \frac{dM}{dt} + p_{m0} \lambda e^{-\lambda t}$$
(B.10)

with initial condition  $d_{\rm m}=d_{\rm m0}$ . The solution to the above can be expressed in integral form as

$$d_{\rm m} = d_{m0} + p_{m0} \frac{1 + kR_p}{1 + kR_d} \left( 1 - e^{-\lambda t} \right) + \frac{k \left( R_d - R_p \right)}{1 + kR_d} p_{m0} \int_0^t \left( \frac{M(s)}{M(t)} \right)^{1 + kR_d} \lambda e^{-\lambda s} \, ds, \quad (B.11)$$

which in turn can be rewritten as

$$d_{\rm m} = d_{m0} + p_{m0} \frac{1 + R_p}{1 + R_d} \left( 1 - e^{-\lambda t} \right)$$

$$+ \frac{R_d - R_p}{1 + R_d} p_{m0} \int_0^t \left[ \frac{1 - k}{1 + kR_d} + \frac{k(1 + R_d)}{1 + kR_d} \left( \frac{M(s)}{M(t)} \right)^{1 + kR_d} \right] \lambda e^{-\lambda s} \, ds.$$
 (B.12)

A convenient way of rewriting the integral in the above expression is in terms of an age distribution (see section E for further discussion of age distributions). Let  $T_d$  be a random variable with cumulative distribution function (CDF)

$$\mathbb{P}(T_d \le s) = \frac{1 - k}{1 + kR_d} + \frac{k(1 + R_d)}{1 + kR_d} \left(\frac{M(s)}{M(t)}\right)^{1 + kR_d}, \qquad 0 < s < t$$
 (B.13)

with  $\mathbb{P}(T_d \leq s) = 0$  for s < 0 and  $\mathbb{P}(T_d \leq s) = 1$  for s > t. The corresponding probability density function (PDF) is

$$\rho(s) = \frac{1 - k}{1 + kR_d} \delta(s) + k(1 + R_d) \left(\frac{M(s)}{M(t)}\right)^{kR_d} \frac{\dot{M}(s)}{M(t)},\tag{B.14}$$

where  $\delta(s)$  is the Dirac delta function.  $\rho(s) = 0$  for s < 0 and s > t. The integral expression on the right hand side of (B.12) is thus

$$\int_{0}^{t} \mathbb{P}(T_d \le s) \lambda e^{-\lambda s} ds = \int_{0-}^{t} \rho(s) \left( e^{-\lambda t} - e^{-\lambda s} \right) ds = \mathbb{E} \left( e^{-\lambda t} - e^{-\lambda T_d} \right)$$
(B.15)

where  $\mathbb{E}$  denotes expectation. Thus we can write (B.12) more compactly as

$$d_{\rm m} = d_{m0} + p_{m0} \frac{1 + R_p}{1 + R_d} \left( 1 - e^{-\lambda t} \right) + \frac{R_p - R_d}{1 + R_d} p_{m0} \mathbb{E}(e^{-\lambda T_d} - e^{-\lambda t}).$$
 (B.16)

Consider now a stable reference isotope d', which is of the same element as d but neither decays nor is a decay product. Thus  $d'_{\rm m} = d'_{\rm m0}$ . Since

$$\left(\frac{d}{d'}\right)_{m0} = \left(\frac{d}{d'}\right)_{b0}, \qquad \left(\frac{p}{d'}\right)_{m0} = \frac{1 + R_d}{1 + R_p} \left(\frac{p}{d'}\right)_{b0}, \tag{B.17}$$

on dividing (B.16) by  $d'_{\rm m}$  we have

$$\left(\frac{d}{d'}\right)_{\mathrm{m}} = \left(\frac{d}{d'}\right)_{\mathrm{b0}} + \left(\frac{p}{d'}\right)_{\mathrm{b0}} \left(1 - \mathrm{e}^{-\lambda t}\right) + \left[\left(\frac{p}{d'}\right)_{\mathrm{m0}} - \left(\frac{p}{d'}\right)_{\mathrm{b0}}\right] \mathbb{E}(\mathrm{e}^{-\lambda T_d} - \mathrm{e}^{-\lambda t}). \tag{B.18}$$

Since the bulk evolution satisfies

$$\left(\frac{d}{d'}\right)_{b} = \left(\frac{d}{d'}\right)_{b0} + \left(\frac{p}{d'}\right)_{b0} \left(1 - e^{-\lambda t}\right),\tag{B.19}$$

(B.18) can be rewritten as

$$\frac{(d/d')_{\rm m} - (d/d')_{\rm b}}{(p/d')_{\rm m0} - (p/d')_{\rm b0}} = \mathbb{E}(e^{-\lambda T_d} - e^{-\lambda t})$$
(B.20)

or

$$\frac{(d/d')_{\rm m} - (d/d')_{\rm b}}{(p/d')_{\rm m} - (p/d')_{\rm b}} = \mathbb{E}(e^{\lambda(t - T_d)} - 1).$$
(B.21)

(B.20) is the more useful form for extinct isotope systems such as Hf-W, since the present day concentrations of the parent isotope are negligible. Given a reference isotope p' for the parent, (B.20) may be rewritten as

$$\frac{(d/d')_{\rm m} - (d/d')_{\rm b}}{(p/p')_{\rm b0} [(p'/d')_{\rm m} - (p'/d')_{\rm b}]} = \mathbb{E}(e^{-\lambda T_d} - e^{-\lambda t}),$$
(B.22)

which is similar to the usual form in which Hf-W model ages are expressed. For extinct systems like Hf-W,  $e^{-\lambda t}$  is essentially zero at the present day. (B.20), (B.21), and (B.22) are very similar to the usual expressions for a two stage model age. Indeed, the aim of introducing the random variable  $T_d$  is to make this similarity clear. The usual expressions for a two stage age with full equilibration drop the expectations and have  $T_d$  replaced by the equilibrium two stage age  $t_{2,eq}$ . Thus

$$\mathbb{E}(e^{-\lambda T_d}) = e^{-\lambda t_{2,eq}}.$$
(B.23)

# C Relationships between model ages

(B.23) is the fundamental equation for comparing different model ages. The equilibrium two stage age on the right hand side can be estimated from the current mantle and bulk compositions. The left hand side depends on the accretion rate through M(t), the amount of equilibration through k, and the enrichment of the daughter isotope in the metal during partitioning through  $R_d$ . Different models assume different forms for M(t), and different amounts of equilibration k. To compare the different models, we must study the behaviour of  $\mathbb{E}(e^{-\lambda T_d})$ . Different models should give equal values for this quantity in order to fit the same observations. Note that for long lived isotope systems such as U-Pb,  $\mathbb{E}(e^{-\lambda T_d}) \approx 1 - \lambda \mathbb{E}(T_d)$ , and thus for such systems  $\mathbb{E}(T_d)$  takes the same value between different models. It is convenient to introduce a new random variable  $S_d$  with cumulative distribution function

$$\mathbb{P}(S_d \le s) = (M(s))^{1+kR_d}, \qquad s > 0$$
 (C.1)

which is related to  $T_d$  by (B.13)

$$\mathbb{P}(T_d \le s) = \frac{1-k}{1+kR_d} + \frac{k(1+R_d)}{1+kR_d} \mathbb{P}(S_d \le s), \qquad s > 0.$$
 (C.2)

In the above it has been assumed that we are considering the present day, where accretion is complete (M(t) = 1). It follows that

$$\mathbb{E}(1 - e^{-\lambda T_d}) = \frac{k(1 + R_d)}{1 + kR_d} \mathbb{E}(1 - e^{-\lambda S_d}), \tag{C.3}$$

$$\mathbb{E}(T_d) = \frac{k(1+R_d)}{1+kR_d} \mathbb{E}(S_d). \tag{C.4}$$

From (C.3) it follows that if we know  $\mathbb{E}(e^{-\lambda T_d})$ , we know  $\mathbb{E}(e^{-\lambda S_d})$ . Models that differ only in the form of M(t) must share the same value of  $\mathbb{E}(e^{-\lambda S_d})$  in order to be compatible with the same observations. However, models that differ in the degree of equilibration k will have different values of  $\mathbb{E}(e^{-\lambda S_d})$ , but will still have the same values of  $\mathbb{E}(e^{-\lambda T_d})$ .

### C.1 Two stage ages

The simplest model is a two stage model, where there is no accretion until a certain time, and then all the accretion occurs at once. The function M(t) is then a step function,

$$M(t) = \begin{cases} 0, & 0 < t < t_2, \\ 1, & t > t_2, \end{cases}$$
 (C.5)

where  $t_2$  is the corresponding two stage age. For the above choice of M(t) we have

$$\mathbb{E}(e^{-\lambda S_d}) = e^{-\lambda t_2},\tag{C.6}$$

$$\mathbb{E}(S_d) = t_2. \tag{C.7}$$

Thus we can relate the two stage age  $t_{2,eq}$  that occurs with full equilibration (k = 1) with a two stage age  $t_2$  that occurs with partial equilibration (0 < k < 1) using (B.23), (C.3), and (C.6)

$$1 - e^{-\lambda t_{2,eq}} = \frac{k(1 + R_d)}{1 + kR_d} \left( 1 - e^{-\lambda t_2} \right).$$
 (C.8)

This relationship is plotted in Figure 3b. It can be approximated for long-lived systems as

$$t_{2,\text{eq}} \approx \frac{k(1+R_d)}{1+kR_d}t_2.$$
 (C.9)

For general  $\lambda$ , Jensen's inequality on (B.23) combined with (C.4) and (C.7) implies

$$t_{2,\text{eq}} \le \mathbb{E}(T_d) = \frac{k(1+R_d)}{1+kR_d} t_2 \le t_2,$$
 (C.10)

and hence disequilibrium always increases the two stage age. From (C.8), the following inequality holds for k,

$$\frac{1 - e^{-\lambda t_{2,eq}}}{1 + R_d e^{-\lambda t_{2,eq}}} \le k \le 1,$$
(C.11)

and hence there is a lower bound on the amount of disequilibrium. These inequalities become equalities as  $\lambda t_2 \to \infty$ , and  $t_2 \to t_{2,eq}$  respectively.

### C.2 Exponential accretion

One of the simplest continuous models of accretion is to assume an exponential accretion with a mean age  $\tau_a$ , namely

$$M(t) = 1 - e^{-t/\tau_a}$$
. (C.12)

The relevant moments are

$$\mathbb{E}(e^{-\lambda S_d}) = \frac{\Gamma(2 + kR_d)\Gamma(1 + \lambda \tau_a)}{\Gamma(2 + kR_d + \lambda \tau_a)},$$
(C.13)

where  $\Gamma(x)$  is the gamma function, and

$$\mathbb{E}(S_d) = \tau_a H_{1+kR_d},\tag{C.14}$$

where  $H_x$  is the  $x^{\text{th}}$  harmonic number, which can be expressed for general x as  $H_x = \gamma + \Psi(1+x)$ , where  $\gamma$  is the Euler-Maschoroni constant, and  $\Psi$  is the digamma function.

Comparing the expressions for  $\mathbb{E}(e^{-\lambda S_d})$  in (C.6) and (C.13), we see there is the following relationship between the two stage age  $t_2$  and the exponential mean age of accretion  $\tau_a$ ,

$$e^{-\lambda t_2} = \frac{\Gamma(2 + kR_d)\Gamma(1 + \lambda \tau_a)}{\Gamma(2 + kR_d + \lambda \tau_a)},$$
(C.15)

and this used in plotting Figure 3a. It can be approximated for long lived systems using (C.7) and (C.14) as

$$t_2 \approx \tau_a H_{1+kR_d}.\tag{C.16}$$

For long-lived systems, the two stage age is thus always greater than the exponential mean age of accretion,  $t_2 \geq \tau_a$ . However, in general, the two stage age can be less than or greater than the mean age of accretion depending on  $kR_d$  and  $\lambda$ . Independent of  $\lambda$ , the ages satisfy  $t_2 \leq \tau_a H_{1+kR_d}$ , by Jensen's inequality on (C.6). Typical values are  $R_W \sim 16$  and  $R_{Pb} \sim 7$  which give  $H_{1+R_W} \sim 3.4$  and  $H_{1+R_{Pb}} \sim 2.7$ . Thus with full equilibration (k=1) the two stage model ages for Hf-W and U-Pb are around 3 times larger than the exponential model ages, i.e. the two stage model ages relate to the point of  $\sim 95\%$  accretion in the exponential models ( $1 - e^{-3} = 0.95$ ).

For integer values of  $kR_d$ , (C.15) can be expanded as (exploiting the fact that  $\Gamma(x) = (x-1)!$  for integer x)

$$e^{-\lambda t_2} = \prod_{r=1}^{1+kR_d} \left(1 + \frac{\lambda \tau_a}{r}\right)^{-1}$$
 (C.17)

and rewritten as

$$t_2 = \frac{1}{\lambda} \sum_{r=1}^{1+kR_d} \log\left(1 + \frac{\lambda \tau_a}{r}\right) \tag{C.18}$$

which agrees with the relationship quoted by Jacobsen<sup>1</sup> (his equation (77)) in the case of full equilibration. (C.15) is more general as it encompasses partial equilibration, and holds for non-integer values of the parameters.

### C.3 Weibull accretion

A useful two parameter accretion model is

$$M(t) = 1 - e^{-(t/\alpha)^{\beta}},$$
 (C.19)

which is known as the Weibull distribution with time scale parameter  $\alpha$  and shape parameter  $\beta$ . The corresponding mean age of accretion is  $\alpha\Gamma(1+1/\beta)$ . The Weibull distribution encompasses both the models described above for appropriate choices of the shape parameter:  $\beta = 1$  is the exponential model, and as  $\beta \to \infty$  the step function is recovered. For the Weibull model there are no simple closed form expressions for the moments  $\mathbb{E}(e^{-\lambda S_d})$  and  $\mathbb{E}(S_d)$ , and the integrals need to be evaluated numerically (Figure 2).

Weibull models with  $\beta \leq 1$  have their maximum rates of accretion  $(\mathrm{d}M/\mathrm{d}t)$  at time t=0, while Weibull models with  $\beta > 1$  have their maximum rates of accretion at later times t>0. To get a match between Hf-W and U-Pb with a Weibull model,  $\beta < 1$  is required (Figure 2), but this does not imply that Earth's accretion was actually at its most rapid at time 0 (the time of CAI formation). Physical models suggest there may have been a very early stage of slow accretion, followed by rapid accretion and finally a very slow and protracted late accretion  $^{27}$ . If the duration of the very early stage of slow accretion was significantly shorter than the half life of  $^{182}$ Hf then it would have had little influence on the subsequent isotopic evolution. A very early stage of slow accretion could be added to the model without influencing the main result: namely that a stage of rapid early accretion followed by a stage of protracted late accretion is required.

## D Bounds on accretion

#### D.1 Analytical bounds

There are some general bounds that can be placed on the accretion curve M(t) without assuming any particular parametric form. Markov's inequality applied to  $e^{-\lambda S_d}$  is

$$\mathbb{P}(e^{-\lambda S_d} \ge e^{-\lambda t}) \le \frac{\mathbb{E}(e^{-\lambda S_d})}{e^{-\lambda t}}$$
(D.1)

which implies

$$\mathbb{P}(S_d \le t) \le e^{\lambda t} \mathbb{E}(e^{-\lambda S_d}) = e^{\lambda(t - t_2)}, \tag{D.2}$$

and thus the following bound can be placed on M(t) using (C.1),

$$M(t) \le e^{\lambda(t-t_2)/(1+kR_d)},\tag{D.3}$$

which bounds the early accretion ( $t \le t_2$ , Figure 4). Notably, the accretion cannot finish until  $t \ge t_2$ . This bound is achieved by step function accretion curves of the form

$$M(t) = \begin{cases} 0, & 0 < t < t_c, \\ e^{\lambda(t_c - t_2)/(1 + kR_d)}, & t_c < t < \infty, \end{cases}$$
 (D.4)

for  $t_c \leq t_2$ .

Applying Markov's inequality to  $1 - e^{-\lambda S_d}$  gives

$$\mathbb{P}(1 - e^{-\lambda S_d} \ge 1 - e^{-\lambda t}) \le \frac{\mathbb{E}(1 - e^{-\lambda S_d})}{1 - e^{-\lambda t}} \tag{D.5}$$

which implies

$$\mathbb{P}(S_d \le t) \ge \frac{\mathbb{E}(e^{-\lambda S_d}) - e^{-\lambda t}}{1 - e^{-\lambda t}} = \frac{e^{-\lambda t_2} - e^{-\lambda t}}{1 - e^{-\lambda t}},$$
(D.6)

and thus the following bound can be placed on M(t),

$$M(t) \ge \left(\frac{e^{-\lambda t_2} - e^{-\lambda t}}{1 - e^{-\lambda t}}\right)^{1/(1 + kR_d)},$$
 (D.7)

which bounds the late accretion ( $t \ge t_2$ , Figure 4). This bound is achieved by step function accretion curves of the form

$$M(t) = \begin{cases} \left(\frac{e^{-\lambda t_2} - e^{-\lambda t}}{1 - e^{-\lambda t}}\right)^{1/(1 + kR_d)}, & 0 < t < t_c, \\ 1, & t > t_c, \end{cases}$$
(D.8)

for  $t_c \geq t_2$ .

Bounds can also be placed on the mean age of accretion. Let  $T_{\rm acc}$  be a random variable with CDF M(t). Then, from the inequality,

$$1 - (M(t))^n \le n (1 - M(t)), \qquad n \ge 1$$
 (D.9)

it follows that

$$\mathbb{E}(S_d) \le (1 + kR_d)\mathbb{E}(T_{\text{acc}}),\tag{D.10}$$

where  $\mathbb{E}(T_{\rm acc})$  is the mean age of accretion. Similarly, from the inequality

$$1 - (M(t))^n \ge 1 - M(t), \qquad n \ge 1$$
 (D.11)

it follows that

$$\mathbb{E}(S_d) \ge \mathbb{E}(T_{\text{acc}}). \tag{D.12}$$

Jensen's inequality implies that

$$\mathbb{E}(e^{-\lambda S_d}) \ge e^{-\lambda \mathbb{E}(S_d)}.$$
 (D.13)

Since  $\mathbb{E}(e^{-\lambda S_d}) = e^{-\lambda t_2}$ , it follows that

$$t_2 \le \mathbb{E}(S_d). \tag{D.14}$$

Thus the mean age of accretion can be bounded by

$$\frac{t_2}{1 + kR_d} \le \frac{\mathbb{E}(S_d)}{1 + kR_d} \le \mathbb{E}(T_{\text{acc}}) \le \mathbb{E}(S_d). \tag{D.15}$$

For long-lived systems  $\mathbb{E}(S_d) \approx t_2$ , and the two stage age  $t_2$  is then an approximate upper bound on the mean age of accretion.

### D.2 Numerical bounds

Bounds on the accretion curve M(t) can also be calculated numerically. Suppose M(t) is discretised as a sequence of steps, with  $M(t) = M_i$  for  $t_{i-1} < t < t_i$ , where  $t_1 \le t_2 \cdots \le t_n$  are the given times of the steps. Bounding M(t) is then a matter of solving a nonlinear optimisation problem: Minimising or maximising  $M_i$  for a given j subject to the constraints

$$0 \le M_1 \le M_2 \le \cdots M_n \le 1,\tag{D.16}$$

$$1 - e^{-\lambda t_2} = \sum_{i=1}^{n} \left( e^{-\lambda t_{i-1}} - e^{-\lambda t_i} \right) \left( 1 - M_i^{1+kR_d} \right).$$
 (D.17)

(D.16) ensures the accretion curve is valid, and (D.17) ensures the isotopic observations are matched. The above problem can be solved using standard optimisation algorithms. The advantage of a numerical solution is that multiple constraints can be included, and thus bounds that include both Hf-W and U-Pb constraints can be calculated (yellow region, Figure 4). A similar method can be used to numerically calculate bounds on the mean age of accretion using the objective function

$$\sum_{i=1}^{n} (t_i - t_{i-1}) (1 - M_i)$$
(D.18)

and the same constraints.

# E Interpretation of age distributions

Age distributions were introduced in section B in order to represent various integral expressions in a more compact form. However, it should be noted that these age distributions arise naturally from residence time theory, which treats transitions between reservoirs as a Poisson process  $^{33,34}$ . This can be best illustrated for the equilibrium case (k = 1). Conservation of mass for a stable species in the mantle reservoir (A.3) can be written as

$$\frac{\mathrm{d}n_{\mathrm{m}}}{\mathrm{d}t} = c_{\mathrm{b}} \frac{\mathrm{d}M}{\mathrm{d}t} - \frac{R_{c}}{M} \frac{\mathrm{d}M}{\mathrm{d}t} n_{\mathrm{m}} \tag{E.1}$$

where  $n_{\rm m} = (1 - F)Mc_{\rm m}$ , the relative number of moles in the mantle reservoir. In terms of residence time theory, we can identify

$$\mathbb{P}(\mathbf{m} \to \mathbf{c}) = \frac{R_c}{M} \frac{\mathrm{d}M}{\mathrm{d}t} \delta t \tag{E.2}$$

as the probability that an atom in Earth's mantle reservoir will transition to Earth's core reservoir in a time interval  $\delta t$ . This probability varies in time, and is zero once accretion has ceased. By integration, we find that the probability that an atom which was in the Earth's mantle reservoir at time t is still in the Earth's mantle by the end of accretion is

$$\mathbb{P}(\text{atom in m at present}|\text{atom in m at time }t) = (M(t))^{R_c}. \tag{E.3}$$

At time t, the number of atoms which arrive in Earth's mantle reservoir in a time interval  $\delta t$  is

$$c_{\rm b} \frac{\mathrm{d}M}{\mathrm{d}t} \delta t$$
 (E.4)

of which

$$c_{\rm b} \frac{\mathrm{d}M}{\mathrm{d}t} \left( M(t) \right)^{R_c} \delta t \tag{E.5}$$

will remain in Earth's mantle at the end of accretion. Hence

$$\rho(t) = (1 + R_c) \frac{\mathrm{d}M}{\mathrm{d}t} (M(t))^{R_c}$$
(E.6)

is a probability density function which gives the probability that an atom in Earth's mantle at present arrived there at time t. The corresponding cumulative distribution function is

$$\mathbb{P}(T_c \le t) = (M(t))^{1+R_c}. \tag{E.7}$$

Alternatively,  $t - T_c$  is a random variable which gives the amount of time an atom has spent in the mantle reservoir, i.e. it is a random variable giving the distribution of residence times in the mantle reservoir. It is this residence time information for the daughter element which gets encoded in the isotopic observations.

Interpreting the age distributions in the general non-equilibrium (k < 1) case (i.e. (B.13)) is less straightforward, but essentially represents a mixture of unequilibrated zero age material and equilibrated material with a distribution of ages similar to the above.

# F Isotopic parameters and calculated model ages

The Hf-W isotopic system consists of parent  $p={}^{182}{\rm Hf}$ , daughter  $d={}^{182}{\rm W}$ , and reference isotopes  $p'={}^{180}{\rm Hf}$  and  $d'={}^{184}{\rm W}$ . Numerical values for the parameters describing the Hf-W isotopic system are given in Supplementary Table 1. These values yield an equilibrium two stage age  $t_{2,\rm eq}=31.0\pm4.4$  Myr and equilibrium exponential accretion time  $\tau_{a,\rm eq}=10.6\pm0.5$  Myr, assuming constant partition coefficients. The predominant uncertainty is in the Hf/W value of the mantle relative to that of the bulk, which leads to an uncertainty in the assumed constant partition coefficient,  $D_{\rm W}=32.5\pm11.0$ . Hf is thought not to enter the core, and thus  $D_{\rm Hf}=0$ 

The U-Pb isotopic system consists of two parent isotopes  $p = ^{238}$ U,  $^{235}$ U, with respective daughter isotopes  $d = ^{206}$ Pb,  $^{207}$ Pb and common reference isotope  $d' = ^{204}$ Pb. Numerical values for the parameters describing the U-Pb isotopic system are given in Supplementary Table 2. The mantle  $(^{206}$ Pb/ $^{204}$ Pb)<sub>m</sub> and  $(^{207}$ Pb/ $^{204}$ Pb)<sub>m</sub> isotopic ratios are not well constrained, as U/Pb fractionation has been ongoing in the Earth due to crust/mantle differentiation. Different literature estimates for the bulk silicate Earth lead isotopic composition are given in Supplementary Table 3 (after Halliday<sup>15</sup>). As was pointed out by Kamber and Kramers<sup>20</sup>, using some of the estimates in Supplementary Table 3 to calculate a two stage age is circular, as some of the authors assumed a particular two stage age from the outset when constructing their estimates  $^{35,36}$ . However, not all of the estimates are circular, and they still provide a reasonable guide to the uncertainties involved  $^{37}$ .

Unfortunately, the  $(^{238}\text{U}/^{204}\text{Pb})_b \equiv \mu_b$  isotopic ratio of the bulk Earth is not well constrained either, due to the volatility of lead. Estimates of  $\mu_b$  range from  $0.7^{17}$ - $1.4^{38}$ . The mantle value is better constrained, with  $\mu_m = 7-9$  being a typical estimate <sup>17</sup>. These estimates imply a range for the lead partition coefficient,  $D_{\text{Pb}} = 8-25$ . Wood et al. <sup>28</sup> have suggested a value of  $D_{\text{Pb}} \sim 13$  based on experimental partitioning studies, and this is the

value adopted here (and used in the calculations for Figures 2, 3, and 4). It is assumed that U does not enter the core to any great extent, so  $D_{\rm U}=0$ .

Given the partition coefficient estimate  $D_{\rm Pb}=13$ , the estimates of  $(^{206}{\rm Pb}/^{204}{\rm Pb})_{\rm m}$  and  $(^{207}{\rm Pb}/^{204}{\rm Pb})_{\rm m}$  can be combined with the parameters in Supplementary Table 2 to infer the model ages  $t_{2,\rm eq}$  and  $\tau_{a,\rm eq}$ , along with  $\mu_{\rm b}$  and  $\mu_{\rm m}$ . This is done in Supplementary Table 3. The values estimated for  $\mu_{\rm b}$  and  $\mu_{\rm m}$  are broadly consistent with the estimates above. There is a wide range in the estimated model ages,  $t_{2,\rm eq}=55.9-130.5$  Myr and  $\tau_{a,\rm eq}=21.6-51.0$  Myr (using all but the two most extreme estimates from Supplementary Table 3), but nevertheless the ages are notably different from those obtained for Hf-W. The bounds of Figure 4 are calculated using a U-Pb two stage age of  $t_{2,\rm eq}=65.0$  Myr, but it should be noted that this is simply chosen as a reasonably reasonably representative value, to illustrate the kind of constraints that Pb isotopes provide, and is not a definitive value.

# G Parametrisation of metal/silicate partition coefficients

Metal/silicate partition coefficients depend on temperature, pressure, and oxygen fugacity conditions. Here we have used the metal/silicate partition coefficient parametrisation of Wade and Wood<sup>6,7,28,29</sup>, which is outlined below. For a fuller description the reader is referred to the original papers.

Oxygen fugacity is defined relative the iron-wüstite (IW) buffer as

$$\Delta IW = 2\log_{10}\left(\gamma_{\text{FeO}}^{\text{sil}}/\gamma_{\text{Fe}}^{\text{met}}\right) + 2\log_{10}\left(x_{\text{FeO}}^{\text{sil}}/x_{\text{Fe}}^{\text{met}}\right),\tag{G.1}$$

where  $\Delta IW$  is the oxygen fugacity relative to the IW buffer in  $\log_{10}$  units.  $\gamma_{\rm Fe}^{\rm met}$  and  $\gamma_{\rm FeO}^{\rm sil}$  are the activity coefficients of Fe and FeO in the metal and silicate respectively, and  $x_{\rm Fe}^{\rm met}$  and  $x_{\rm FeO}^{\rm sil}$  are the corresponding molar concentrations. The activity coefficients of elements in the metal phase are assumed to depend on temperature as

$$\gamma_{\mathcal{M}}^{\text{met}}(T) = \left(\gamma_{\mathcal{M}}^{\text{met}}(T_0)\right)^{T_0/T} \tag{G.2}$$

where  $\gamma_{\rm M}^{\rm met}(T_0)$  is the activity at a reference temperature of  $T_0=1873$  K. Formally, the activity coefficients should also depend on pressure and composition, but for simplicity this dependence is neglected here, and  $\gamma_{\rm M}^{\rm met}(T_0)$  is assumed constant. The activities  $\gamma_{\rm M}^{\rm met}(T_0)$  at the reference temperature were calculated by an interaction parameter approach<sup>39</sup>, with an assumed metal composition, and are given in Supplementary Table 4. The activity of FeO in the silicate is assumed to be independent of temperature, with  $\gamma_{\rm FeO}^{\rm sil}=3$ . Different choices for  $\gamma_{\rm FeO}^{\rm sil}$  affect the absolute values of the oxygen fugacity, but the relative results will remain the same.

Using (G.1) and (G.2), the molar Fe metal/silicate partition coefficient can be written as a function of oxygen fugacity as

$$\log_{10} D_{\text{Fe}}^{\star} \equiv \log_{10} \left( x_{\text{Fe}}^{\text{met}} / x_{\text{FeO}}^{\text{sil}} \right) = -\frac{1}{2} \Delta IW - \frac{T_0}{T} \log_{10} \gamma_{\text{Fe}}^{\text{met}} (T_0) + \log_{10} \gamma_{\text{FeO}}^{\text{sil}}. \tag{G.3}$$

The partitioning of the other elements is parametrised relative to the iron partitioning as

$$\log_{10} D_{\mathrm{M}}^{\star} = a + b \frac{1}{T} + c \frac{P}{T} + dN + \frac{v}{2} \log_{10} D_{\mathrm{Fe}}^{\star} + \frac{T_0}{T} \left( \frac{v}{2} \log_{10} \gamma_{\mathrm{Fe}}^{\mathrm{met}}(T_0) - \log_{10} \gamma_{\mathrm{M}}^{\mathrm{met}}(T_0) \right)$$
 (G.4)

which can be rewritten as

$$\log_{10} D_{\rm M}^{\star} = a + b \frac{1}{T} + c \frac{P}{T} + dN - \frac{v}{4} \Delta IW - \frac{T_0}{T} \log_{10} \gamma_{\rm M}^{\rm met}(T_0) + \frac{v}{2} \log_{10} \gamma_{\rm FeO}^{\rm sil}.$$
 (G.5)

a, b, c, and d are coefficients obtained by regression of experimental data, given in Supplementary Table 4. v is the assumed valence (which for W is also found by regression as it has mixed valence states  $^{30}$ ). T is the temperature (in K), P is the pressure (in GPa), and N is the molar ratio of non-bridging oxygens to tetrahedral cations in the silicate melt (assumed constant at 2.7). (G.3), (G.4), and (G.5) parametrise the molar partition coefficients  $D_{\rm M}^{\star}$ , but what is of usual interest is the partition coefficients by mass, namely

$$D_{\rm M} = c_{\rm M}^{\rm met}/c_{\rm M}^{\rm sil},\tag{G.6}$$

where c refers to concentration by mass. However, to a good approximation it is found that  $D_{\rm M} \approx D_{\rm M}^{\star}$ , and we will use molar and mass partition coefficients interchangeably.

Target values for the partition coefficients can be obtained from estimates of the present day mantle  $c_{\rm m}$  and core  $c_{\rm c}$  abundances, namely

$$D^{\text{obs}} = c_{\text{c}}/c_{\text{m}}.\tag{G.7}$$

Estimated values are given in Supplementary Table 5. Note that these target values should be compared to integrated values of the true partition coefficients over the different pressure, temperature, and oxygen fugacity conditions that have been experienced during metal silicate-equilibration over the course of the Earth's accretion.

# H Pressure, temperature, and oxygen fugacity evolution

To complete the model, the pressure, temperature and oxygen fugacity conditions under which metal silicate equilibration takes place must be specified. The approach taken here is based on that of Wade and Wood<sup>6</sup>, where it postulated that the point of last metal-silicate equilibration takes place at the base of a deep magma ocean. This final metal-silicate equilibration is assumed to take place on the peridotite liquidus, which we approximate by

$$T = 1973 + 28.57P, (H.1)$$

where T is in K and P is in GPa. The pressure of equilibration is assumed to evolve as

$$P(t) = P_0(M(t))^{2/3},$$
 (H.2)

for some constant  $P_0$  to be determined. The assumed scaling of  $(M(t))^{2/3}$  reflects the increase in pressure with planet size, which scales as the square of the planet radius. The pressure  $P_0$  can be associated with an average depth of magma ocean equilibration through  $h_0/h_{\rm cmb} = P_0/P_{\rm cmb}$ , where  $P_{\rm cmb}$  and  $h_{\rm cmb}$  are the present day core-mantle boundary pressure and depth  $(P_{\rm cmb} = 135 \text{ GPa}, h_{\rm cmb} = 2886 \text{ km})$ .

Finally, the oxygen fugacity state is allowed to evolve as the planet accretes. We assume the following simple form, based on that of Corgne et al<sup>7</sup>,

$$\Delta IW = \begin{cases} \Delta IW_1, & 0 < M(t) < 0.1, \\ \Delta IW_1 + (\Delta IW_2 - \Delta IW_1) \frac{M(t) - 0.1}{0.9}, & 0.1 < M(t) < 1, \end{cases}$$
(H.3)

for initial oxygen fugacity  $\Delta IW_1$  and final oxygen fugacity  $\Delta IW_2$ . The oxygen fugacity remains constant for the first 10% of the accretion, and then increases linearly for the remainder of the accretion.

#### I Trace element inversion

Values of the parameters  $P_0$ ,  $\Delta IW_1$  and  $\Delta IW_2$  that best fit the observations are obtained by inversion, using a penalty function approach (Figure 1). Having these three free parameters seems to be the minimum needed to get a good match to the observations. The chosen penalty function to minimise is

$$g(P_0, \Delta IW_1, \Delta IW_2) = \sum_{i=1}^{n} \left( \frac{\log_{10} D_i^{\text{model}} - \log_{10} D_i^{\text{obs}}}{\sigma_i} \right)^2$$
 (I.1)

where  $D_i^{\text{model}}$  is the overall partition coefficient that is obtained from integrating the model, namely  $D^{\text{model}} = c_{\text{c}}/c_{\text{m}}$ .  $i = 1, 2, \ldots, n$  refer to the n trace elements that are used for inversion. Only a subset of the available trace elements are used in the inversion (Fe, Ni, Co, V, W, Si, Nb, Ta), since these elements are the most refractory and their bulk Earth abundances are thus best constrained. The uncertainties  $\sigma_i^2$  arise from two sources: uncertainties in the experimentally derived partition coefficients  $D_i^*$ , which lead to uncertainties in  $D_i^{\text{model}}$  on integrating the model (shown as red error bars in Figure 1), and uncertainties in the present day elemental abundances, which lead to uncertainties in  $D_i^{\text{obs}}$  (shown as blue error bars in Figure 1). The total uncertainty is given by

$$\sigma_i^2 = \sigma_{\log_{10} D_i^{\text{model}}}^2 + \sigma_{\log_{10} D_i^{\text{obs}}}^2, \tag{I.2}$$

which is used to weight the different terms in (I.1). The lower the uncertainty, the greater weight that is placed on that term in the penalty function. Thus certain elements influence the penalty function more strongly than others, as some elements have better constrained abundances and partitioning behaviours. The  $1\sigma$  uncertainties on  $\log_{10} D^{\text{obs}}$  are given in Supplementary Table 5, and the  $1\sigma$  uncertainties on the experimental regression coefficients for  $D^*$  are given in Supplementary Table 4. The error propagation to determine the uncertainty on  $D^{\text{model}}$  proceeds under the assumption of independent errors, namely

$$\sigma_{\log_{10} D^{\star}}^{2} = \sigma_{a}^{2} + \sigma_{b}^{2} \frac{1}{T^{2}} + \sigma_{c}^{2} \frac{P^{2}}{T^{2}} + \sigma_{d}^{2} N^{2} + \frac{\sigma_{v}^{2}}{16} \Delta I W^{2}.$$
 (I.3)

Different studies report errors in different ways, which makes comparing errors between studies difficult. For the studies considered here, the most noticeable difference is that Cottrell et al.  $^{30}$  report errors on all regression coefficients (v, a, b, c, d) whereas the other studies  $^{6,7,28,29}$  only report errors on the coefficients c and d (and also b for the case of Cr in  $^{7}$ ). To make a fair comparison between the W partition coefficients of Cottrell et al.  $^{30}$  and the other studies we have used a regression through the Cottrell et al.  $^{30}$  data set which has b set to the value given in thermodynamic tables (as done in the other studies  $^{6}$ ), and have not put any errors on the coefficients a and b. We have kept the error on the valence v as W, unlike the other elements, has a mixed valence state (between 4 and 6), which requires v to be a fitted parameter.

Different elements are sensitive to different model parameters because their partitioning depends in different ways on temperature, pressure, and oxygen fugacity. The inversion

technique is particularly sensitive to the more siderophile elements and to those elements whose uncertainties are smallest, such as Fe, Ni, Co and V. The Fe abundance is best known, and sets the integrated oxygen fugacity. High pressures and an increase in oxygen fugacity are required to simultaneously match the slightly siderophile elements such as V and the more siderophile Ni and Co<sup>6,29</sup>. Increasing oxygen fugacity also seems to be required to get the correct mantle Nb/Ta ratio<sup>7</sup>. In Figure 1, good fits are seen for all elements, with the exception of Ga. The reason for gallium's misfit is unclear, but may be due to a poor assessment of the bulk Earth value as it is volatile<sup>7</sup>.

When disequilibrium models are considered (as in Figure 1b) the conditions of differentiation in the embryos are important and must be specified. There is a trade-off between conditions in the embryos and the inferred conditions during accretion. An example is shown in Supplementary Figure 2 where the oxygen fugacity conditions on Earth are plotted as a function of the oxygen fugacity of differentiation in the embryos. If the conditions in the embryos are sufficiently reducing (in this case  $\Delta IW = -2.7$ ), there is no need for an increase in oxygen fugacity during accretion. It should be noted that the misfit (given by (I.1)) also varies as a function of embryo oxygen fugacity, with a value around -0.5 being the best fitting (lowest misfit), and increasing for values lower than this. However, all the embryo values shown in Supplementary Figure 2 still provide goods fits to the observations to within the uncertainties. It should be noted that Figure 1 and Supplementary Figure 2 assume all embryos differentiate under the same pressure, temperature, and oxygen fugacity conditions. However, it is likely that this is not the case, and one alternative to having an increase in oxygen fugacity during Earth's accretion is to have more oxidised material accreting later<sup>24</sup>.

# J Remarks on partially equilibrative plumbing

The k=1 case of the model presented here is exactly the "fully equilibrative plumbing" model first introduced by Harper and Jacobsen<sup>40</sup>. However, the k<1 and k=0 cases are different from the "partially equilibrative plumbing" and "non-equilibrative plumbing" models of Harper and Jacobsen<sup>40</sup>. Partial and non-equilibrative plumbing have metal-silicate equilibration in the embryos occurring at the time of accretion rather than at time 0 as happens here. This can be investigated in the same way, by changing the concentrations in the incoming material from those given in (B.8) to

$$d_{\text{me}} = \frac{1}{1 + R_d} \cdot \frac{d_{b0} + p_{b0}(1 - e^{-\lambda t})}{1 - F},$$
 (J.1)

$$d_{\rm ce} = \frac{R_d}{1 + R_d} \cdot \frac{d_{\rm b0} + p_{\rm b0}(1 - e^{-\lambda t})}{F}.$$
 (J.2)

Following through the same calculations as before, the cumulative distribution function associated with the partially equilibrative plumbing model is simply

$$\mathbb{P}(T_d \le t) = (M(t))^{1+kR_d}, \qquad (J.3)$$

which is exactly the same as the distribution of  $S_d$  encountered earlier. Hence all the relationships derived for  $S_d$  can be applied directly to the partially equilibrative plumbing model. It should be noted that the two stage age  $t_2$  is independent of the degree of equilibration k

for the partially equilibrative plumbing model,  $t_2 = t_{2,eq}$ . However, the exponential mean age certainly does depend on k, through

$$e^{-\lambda t_{2,eq}} = e^{-\lambda t_2} = \frac{\Gamma(2 + kR_d)\Gamma(1 + \lambda \tau_a)}{\Gamma(2 + kR_d + \lambda \tau_a)}.$$
 (J.4)

For the end-member case of non-equilibrative plumbing (k = 0), the above simplifies to

$$t_{2,\text{eq}} = \frac{1}{\lambda} \log \left( 1 + \lambda \tau_a \right), \tag{J.5}$$

which is the relationship quoted by Jacobsen and Harper <sup>41</sup> (equation (61)) and Harper and Jacobsen <sup>40</sup> (equation (11)).

# K Remarks on the relationship between two stage model ages

The relationship between two stages ages with and without equilibration has also been discussed by Allègre et al.<sup>17</sup>, in which it was found that two stage ages  $t_2 = 110 - 190$  Myr and degrees of equilibration from 0.86 to 0.94 were needed to obtain overlap between Hf-W and U-Pb. While the inferred ages are broadly in line with those estimated here, the degrees of equilibration are not. The relationship between the two stages ages given by Allègre et al.<sup>17</sup> is

$$1 - e^{-\lambda t_{2,eq}} = f_d \left( 1 - e^{-\lambda t_2} \right),$$
 (K.1)

where symbols have been changed to be compatible with the notation of this manuscript. In Allègre et al. <sup>17</sup>,  $t_{2,eq}$  is referred to as the apparent age, and  $t_2$  as the true age, but it should be noted that both ages are examples of model ages.  $f_d$  is referred to as the fraction of silicate exchanged. (K.1) should be compared with (C.8), which implies that  $f_d$  is related to k by

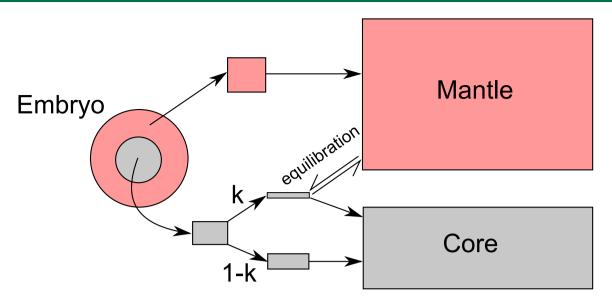
$$f_d = \frac{k(1 + R_d)}{1 + kR_d}. (K.2)$$

The amount of equilibration quoted by Allègre et al. <sup>17</sup> is in terms of  $f_d$  rather than the mass fraction k, with 0.86 to 0.94 being values of  $f_d$  thought to be consistent with the observations. Allègre et al. <sup>17</sup> assume that  $f_d$  is the same for both W and Pb, but as can be seen in (K.2),  $f_d$  depends on  $R_d$  and thus on the partitioning behaviour of the daughter; likely to be different for W and Pb. The error in Allègre et al. <sup>17</sup> arises from a mistake in using the mixing equation for isotopic ratios in the form  $(d/d') = f_d(d/d')_1 + (1 - f_d)(d/d')_2$ . The quantity  $f_d$  in this equation is not the proportion by mass in which the two quantities mix, but depends on the concentrations of the two substances. The values of  $f_d$  quoted by Allègre et al. <sup>17</sup> can be converted to k using (K.2). With a typical value for  $R_W = 15$  ( $D_W = 33$ ), the quoted  $f_d$  values imply a reequilibration mass fraction k of around 0.28 to 0.49.  $R_{\rm Pb}$  is much less well known, but using a value of 6 ( $D_{\rm Pb} = 13$  as used above) implies a reequilibration fraction k of around 0.46 to 0.69. The values of k consistent with both Hf-W and U-Pb estimated here (k = 0.37 - 0.41) lie somewhere in the middle of the values one can infer from Allègre et al. <sup>17</sup>. Conversely, using the k values here, consistency requires  $f_W \approx 0.91$  and  $f_{\rm Pb} \approx 0.81$ .

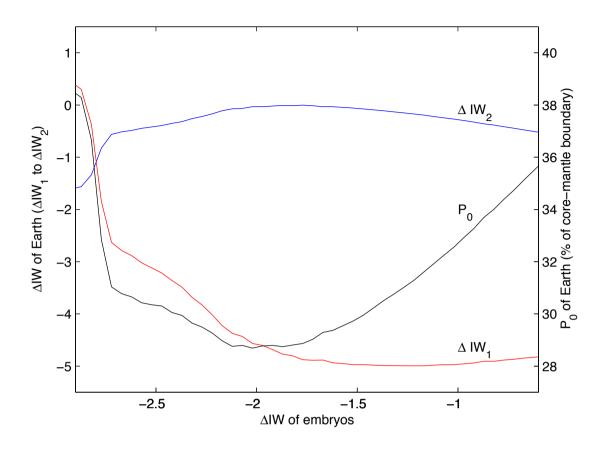
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Supplementary Figure 1: A sketch of the box model used throughout this work. Embryo material differentiates into metal and silicate in equilibrium with one another at time 0. Over the course of the accretion, embryo material is added to the Earth. Embryo mantle material is added directly to the Earth's mantle, whereas embryo core material take two routes: a mass fraction k chemically equilibrates with the Earth's mantle as it travels to the core, and the remaining 1 - k is added directly to the Earth's core without reequilibration.



Supplementary Figure 2: An example of the trade-off between conditions in the embryos and conditions on Earth in a disequilibrium model (k=0.42). The embryos are assumed to differentiate at pressure  $P_{\rm embryo}=9$  GPa, temperature  $T_{\rm embryo}=2700$  K, and oxygen fugacity  $\Delta IW_{\rm embryo}$  as shown on the horizontal axis. The three Earth parameters  $P_0$  (black line),  $\Delta IW_1$  (red line), and  $\Delta IW_2$  (blue line) which best fit the siderophile element abundances are plotted as a function of  $\Delta IW_{\rm embryo}$ . In disequilibrium models, the inferred change in oxygen fugacity is very sensitive to the oxygen fugacity conditions under which the embryos differentiate. In fact, the siderophile element abundances can be explained without an increase in oxygen fugacity over Earth's accretion provided conditions of differentiation in the embryos are sufficiently more reducing than on Earth. In this particular example,  $\Delta IW_{\rm embryo}=-2.8$  and  $\Delta IW_{\rm Earth}=-1.1$  are appropriate values for which an increase in oxygen fugacity during accretion is not required (intersection of the  $\Delta IW_1$  and  $\Delta IW_2$  curves).

Supplementary Table 1: Input parameters for the Hf-W system <sup>12</sup>. These parameters imply an equilibrium two stage model age  $t_{\rm 2eq} = 31.0 \pm 4.4$  Myr and equilibrium mean accretion time  $\tau_{a,\rm eq} = 10.6 \pm 0.5$  Myr. The uncertainty is dominated by the uncertainty in mantle <sup>180</sup>Hf/<sup>184</sup>W.

Parameter	Value	Remarks
λ	$(7.78 \pm 0.02) \times 10^{-8} \text{ yr}^{-1}$	Decay constant of <sup>182</sup> Hf.
${\binom{182}{\text{Hf}}}^{180}{\text{Hf}}_{\text{b0}}$ ${\binom{180}{\text{Hf}}}^{184}{\text{W}}_{\text{b}}$	$(9.72 \pm 0.44) \times 10^{-5}$	Initial bulk Earth value. Derived from internal isochron for CAIs.
	$1.23 \pm 0.15$	Bulk Earth value, based on CAIs and carbonaceous chondrites.
$(^{180}\text{Hf}/^{184}\text{W})_{\text{m}}^{182}$	$20.06 \pm 5.90$	Present day bulk silicate Earth value.
	$0.864699 \pm 0.000012^*$	Present day bulk Earth value (carbonaceous chondrite value).
$(^{182}W/^{184}W)_{\rm m}^{6}$	$0.864863 \pm 0.000018^*$	Present day bulk silicate Earth value (terrestrial standard value).

<sup>\*</sup> Note that the relative difference for  $^{182}W/^{184}W$  between bulk silicate Earth and chondrites is better known that the absolute values of  $^{182}W/^{184}W$  (the difference is  $1.9 \pm 0.1$  in  $\varepsilon_W$  units).

Supplementary Table 2: Input parameters for the U-Pb system

Supplem	ientary Table 2. mpu	t parameters for the O-1 o system.
Parameter	Value	Remarks
$\lambda_{238}$	$1.551 \times 10^{-10} \text{ yr}^{-1}$	Decay constant of <sup>238</sup> U.
$\lambda_{235}$	$9.849 \times 10^{-10} \text{ yr}^{-1}$	Decay constant of <sup>235</sup> U.
$(^{235}U/^{238}U)_{\rm b}$	1/137.88	Present day value.
$(^{206}\text{Pb}/^{204}\text{Pb})_{b0}$	9.307	Initial bulk Earth value (Canyon Diablo).
$(^{207}\text{Pb}/^{204}\text{Pb})_{b0}^{b0}$	10.294	Initial bulk Earth value (Canyon Diablo).

Supplementary Table 3: Estimates of bulk silicate Earth lead isotopic composition with calculated  $\mu$  and model ages (based on Table 1 of Halliday 2004 <sup>15</sup>, but with slightly different model assumptions).  $\mu$  is the present day <sup>238</sup>U/<sup>204</sup>Pb value. Calculated values assume a constant partition coefficient  $D_{\rm Pb}=13^{28}$  and an initial time of 4567 Myr before present. The model ages are not well constrained, ranging from  $t_{2,\rm eq}=53.5-171.0$  Myr and  $\tau_{a,\rm eq}=20.7-67.3$  Myr with this assumed value of the partition coefficient.

Reference	$(^{206}\text{Pb}/^{204}\text{Pb})_{\text{m}}$	$(^{207}\text{Pb}/^{204}\text{Pb})_{\text{m}}$	$\mu_b$	$\mu_m$	$t_{2,\text{eq}}$ (Myr)	$\tau_{a,\text{eq}} \text{ (Myr)}$
Kramers and Tolstikhin 1997 <sup>35</sup>	17.440	15.160	1.13	8.05	74.7	29.0
Kwon et al. 1989 <sup>42</sup>	17.822	15.445	1.18	8.38	55.9	21.6
Davies 1984 <sup>43</sup>	17.830	15.457	1.18	8.39	53.5	20.7
Liew et al. $1991^{44}$	17.920	15.470	1.20	8.51	67.2	26.0
Murphy et al. $2003^{36}$	18.070	15.540	1.22	8.67	73.7	28.6
Galer and Goldstein 1991 <sup>45</sup>	18.110	15.617	1.22	8.67	56.6	21.9
Doe and Zartman 1979 <sup>46</sup>	18.252	15.476	1.26	8.98	130.5	51.0
Kamber and Collerson 1999 <sup>47</sup>	18.270	15.600	1.25	8.91	93.0	36.2
Allègre and Lewin 1989 <sup>48</sup>	18.340	15.551	1.27	9.05	122.5	47.9
Allègre et al. $1988^{49}$	18.400	15.580	1.28	9.12	124.4	48.6
Zartman and Haines 1988 <sup>50</sup>	18.619	15.565	1.33	9.45	171.0	67.3

Supplementary Table 4: Coefficients used in the partition coefficient parametrisation (G.4). Values in brackets are the 1 standard deviation error on the regression coefficients.  $\gamma_{\rm M}^{\rm met}(T_0)$  are the C-unsaturated activity coefficients calculated at a reference temperature of  $T_0=1873$  K using an interaction parameter approach (not used for Ti, Zn, or Pb). P coefficients from are based on unpublished data by M. Walter. Uncertainties on the regression coefficients are not available for P or Pb.

	v	a	b (K)	$c  (\mathrm{KGPa^{-1}})$	d	$\gamma_{ m M}^{ m met}(T_0)$	reference
Mn	2	-0.02	-5600	38 (6)	0.036 (0.010)	0.6473	Corgne et al. 2008 <sup>7</sup>
Ni	2	0.50	3100	-78 (5)	-0.073 (0.015)	0.6819	Corgne et al. $2008^7$
$\operatorname{Cr}$	2	0.09	-2845 (461)	-20 (10)	0.000(0.013)	0.7705	Corgne et al. 2008 <sup>7</sup>
Ga	3	3.50	-4800	-126 (36)	-0.97(0.15)	0.8762	Corgne et al. 2008 <sup>7</sup>
$\operatorname{Si}$	4	2.97	-21800	-11 (33)	-0.24 (0.11)	0.0077	Corgne et al. $2008^7$
Nb	5	4.09	-15500	-166 (31)	-0.75(0.16)	0.1107	Corgne et al. 2008 <sup>7</sup>
Ta	5	7.74	-20000	-264 (81)	-1.69(0.53)	0.1029	Corgne et al. 2008 <sup>7</sup>
$\mathrm{Ti}$	4	3.46	-19000	-42 (52)	-0.11(0.16)	1.0000	Corgne et al. 2008 <sup>7</sup>
Cu	1	0.30	2300	-37(45)	0.14(0.17)	10.9980	Corgne et al. 2008 <sup>7</sup>
Zn	2	-1.11	600	-23 (102)	-0.21 (0.24)	1.0000	Corgne et al. 2008 <sup>7</sup>
V	3	0.855	-8548	-62 (19)	-0.101 (0.029)	0.1076	Wood et al. $2008^{29}$
Co	2	0.01	2511	-45 (11)	0	0.4790	Wade and Wood $2005^6$
P	5	0.64	-1593	-74.95	0	4.2805	Wade and Wood $2005^6$
W	4.52(0.52)	3.2	-1605	-115 (15)	-0.85(0.07)	0.9411	Cottrell et al $2009^{30,51}$
Pb	2	0.788	-2436	0	0	1.0000	Wood et al. $2008^{28}$
Fe	2	0	0	0	0	0.8762	

Supplementary Table 5: Effective partition coefficients inferred from present day core/mantle concentrations,  $D^{\rm obs} = c_{\rm c}^{\rm obs}/c_{\rm m}^{\rm obs}$ . First column shows  $\log_{10} D_{\rm obs}$  with a 1 standard deviation error in brackets. The  $2\sigma$  range for  $D_{\rm obs}$  that results is shown in the second column. Asterixes (\*) denote volatile elements, for which estimates of bulk Earth composition are much more uncertain. Estimates are based on those used by Corgne et al.<sup>7</sup> and Wade and Wood<sup>6</sup> (in turn based on  $^{52-54}$ ) with the exception of W which is based on  $^{12}$ . The volatile and only moderately siderophile elements Zn and Ga have very uncertain abundances. Ti is normally regarded as a refractory lithophile element, and thus its concentration in the core is usually estimated to be zero.

	$\log_{10} D^{\mathrm{obs}}$	$2\sigma$ interval for $D^{\rm obs}$
W	1.513 (0.077)	23-46
Ni	$1.418 \ (0.017)$	24-28
$P^*$	1.398(0.140)	13-48
Co	$1.381\ (0.013)$	23-26
Pb	1.159 (0.118)	8-25
Fe	1.136	13.66
$Cu^*$	$0.801\ (0.099)$	4-10
V	$0.262 \ (0.042)$	1.5 - 2.2
$\mathrm{Cr}^*$	0.195 (0.175)	0.7 - 3.5
$Mn^*$	-0.155 (0.274)	0.2 - 2.5
Nb	-0.276 (0.211)	0.2 - 1.4
Ta	$-0.611 \ (0.195)$	0.1 - 0.6
$Si^*$	-0.728 (0.136)	0.10 - 0.35
$Zn^*$	-0.824 (0.301)	0-0.6
$Ga^*$	-1.000 (0.301)	0-0.4
Ti	$-\infty$	0

#### Supplementary Table 6: Table of variables

```
coefficients used in partition coefficient parametrisation ((G.5) and Supplementary Table 4)
a, b, c, d, v
             concentration of chemical species in the bulk Earth
        c_{\rm b}
             concentration of chemical species in the Earth's core
        c_{\rm c}
             initial concentration of chemical species in the Earth's core (c_c at t=0)
        c_{\rm c0}
             concentration of chemical species in the core of the embryos
        c_{\rm ce}
             concentration of chemical species in the Earth's mantle
        c_{\rm m}
             concentration of chemical species in the mantle of the embryos
       c_{\rm me}
             daughter isotope, e.g. <sup>182</sup>W
         d
             reference isotope, e.g. ^{184}W
         d'
        D
             partition coefficient by mass
       D^*
             partition coefficient by mole
   D^{\text{model}}
             c_{\rm c}/c_{\rm m} from model calculations
     D^{\text{obs}}
             c_{\rm c}/c_{\rm m} from observed abundances (Supplementary Table 5)
         F
             mass fraction of Earth's core (0.323)
             mass fraction of metal that chemically equilibrates during accretion
         k
     M(t)
             fraction of Earth accreted at time t
             molar ratio of non-bridging oxygens to tetrahedral cations in the silicate melt
        N
             parent isotope, e.g. <sup>182</sup>Hf
         p
             reference isotope, e.g. <sup>180</sup>Hf
         p'
         P
             pressure
         R
             = FD/(1 - F)
             random variable defined by (C.1)
             time since beginning of solar system
          t
         t_2
             two stage model age
             two stage model age, assuming full equilibration (k = 1)
      t_{2,\rm eq}
         T
             temperature
        T_d
             random variable defined by (B.13)
             time scale parameter of Weibull distribution
         \alpha
         \beta
             shape parameter of Weibull distribution
             activity coefficient
    \Delta IW
             oxygen fugacity relative to the iron-wüstite buffer in \log_{10} units
         \lambda
             decay constant
             <sup>238</sup>U/<sup>204</sup>Pb isotopic ratio corrected for radioactive decay
         \mu
             standard deviation
         \sigma
             exponential model age (mean age and time of 63% accretion)
        \tau_a
             exponential model age, assuming full equilibration (k=1)
      \tau_{a,eq}
```