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RESEARCH ARTICLE

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Key Points:

- We model the magmatic response to the last deglaciation in Iceland with finite melt ascent velocity
- The model results compared with observations suggest that the melt ascent velocity is likely to be around 100 m/year

Supporting Information:

- Supporting Information S1
- Movie S1
- Data Set S1
- · Data Set S2

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Rate of Melt Ascent Beneath Iceland From the Magmatic Response to Deglaciation

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Abstract Observations of the time lag between the last deglaciation and a surge in volcanic activity in Iceland constrain the average melt ascent velocity to be ≥50 m/year. Although existing theoretical work has explained why the surge in eruption rates increased 5-30-fold from the steady-state rates during the last deglaciation, they cannot account for large variations of Rare Earth Element (REE) concentrations in the Icelandic lavas. Lavas erupted during the last deglaciation are depleted in REEs by up to 70%; whereas existing models, which assume instantaneous melt transport, can only produce at most 20% depletion. Here we develop a numerical model with finite melt ascent velocity and show that the variations of REEs are strongly dependent on the melt ascent velocity. When the average melt ascent velocity is 100 m/year, the variation of La calculated by our model is comparable to that of the observations. In contrast, when the melt ascent velocity is 1,000 m/year or above, the model variation of La becomes significantly lower than observed, which explains why previous models with instantaneous melt transport did not reproduce the large variations. We provide the first model that takes account of the diachronous response of volcanism to deglaciation. We show by comparing our model calculations of the relative volumes of different eruption types (subglacial, finiglacial, and postglacial) and the timing of the bursts in volcanic eruptions with the observations across different volcanic zones that the Icelandic average melt ascent velocity during the last deglaciation is likely to be ~100 m/year.

1. Introduction

Iceland is located where a mantle plume meets the Mid-Atlantic Ridge (White et al., 1992). The mantle plume and the spreading center are responsible for the upwelling of the mantle underneath Iceland, which induces decompression melting in the upper mantle (McKenzie & Bickle, 1988). This decompression melting produces magma that supplies the production of the Icelandic crust and volcanic eruptions. Geological observations indicate that eruption rates in the volcanic zones of Iceland were significantly elevated during a burst of activity that took place after the end of the last major deglaciation (Eason et al., 2015; Maclennan, 2008; Maclennan et al., 2002; Sigvaldason et al., 1992; Sinton et al., 2005; Slater et al., 1998). This period of high productivity, perhaps 30 times or more, may have started about 15 Kyr BP and ended before 9 Kyr BP.

The cause of the surge in eruption rates has been examined by Jull and McKenzie (1996). In their model, postglacial rebound induced by the last deglaciation increases the rate of pressure drop in the upper mantle by up to 50-fold from the steady-state value. This increase in the decompression rate significantly increases the melting rate in the upper mantle, which leads to greater melt supply.

Jull and McKenzie (1996) also showed that the decompression rate due to postglacial rebound has its maximum value at the surface and decays exponentially with depth. This means that the additional melt production in the mantle during the deglaciation occurs mostly at shallow depths. The melts generated at these depths are depleted in Rare Earth Elements (REEs). These additional melts produced during the deglaciation will therefore dilute the concentrations of REEs in the aggregated melts. By assuming that the melt transport is instantaneous, Jull and McKenzie (1996) calculated that the REE concentrations in the melts decrease by around 20% during the last deglaciation compared to melts generated at other times when the ice load is thought to have been close to steady state. However, geological observations indicate that lavas erupted during the surge in volcanic eruption rates are depleted in REEs by up to $\approx 70\%$ (Eason et al., 2015; Maclennan, 2008; Maclennan et al., 2002; Sinton et al., 2005; Slater et al., 1998), which is significantly higher than that calculated by Jull and McKenzie (1996).

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Slater et al. (1998) attempted to account for this mismatch by developing an inverse model similar to that of McKenzie and O'Nions (1991), which used the observed variations of REE concentrations to constrain the melt productivity function. Slater et al. (1998) showed that there exists a melt productivity function that matches the Jull and McKenzie (1996) theoretical variations of the REE concentrations with the geological data. However, in order for such a melt productivity function to exist, model parameters had to be modified including reducing the initial ice sheet radius to 90 km, which is significantly smaller than the likely radius of the ice sheet as inferred from observational studies (Hubbard et al., 2006; Licciardi et al., 2007; Patton et al., 2017; Pétursson et al., 2015; Sigmundsson, 1991).

Maclennan et al. (2002) previously used the relative timing of the last deglaciation and the surge in volcanic eruption rates in the Northern Volcanic Zone (NVZ) of Iceland to estimate that the melt ascent velocity is at least 50 m/year. The Icelandic melt ascent velocity during the mid-Holocene has also been estimated from a time lag of \approx 600 years (Swindles et al., 2017) obtained from the cross correlation between the Icelandic volcanic eruption rates and the change in the atmospheric circulation pattern indicated by sodium concentrations in Greenland Ice Sheet Project 2. This \approx 600-year time lag gives an estimated Icelandic melt ascent velocity of \approx 50–100 m/year during the mid-Holocene.

Here we investigate how the melt ascent velocity in the mantle and the crust influences the variations of REE concentrations. By incorporating a finite rate melt transport model into the model of Jull and McKenzie (1996), we show that variations of REE concentrations depend significantly on the melt ascent velocity. With an appropriate melt ascent velocity, our model demonstrates that the model variations of REE concentrations can be matched with those observed geologically. While Jull and McKenzie (1996) used a very simple ice-load model with a constant ice radius, our model combines an ice-load history with melt generation and transport and therefore enables prediction of the volumes and compositions of melt that are erupted either subglacially or in ice-free settings. This feature of the model allows for direct comparison with geological observations, which use edifice geomorphology and volcanic facies analysis to determine whether an eruption is subglacial or not. Therefore, not only does this work help us understand how melt transport affects REE concentrations and eruption types in different places on Iceland, but also it can be useful as a tool to constrain the melt transport rate.

In the next section, we will begin by considering how the mantle flow responds to deglaciation and use this response to calculate the melting rate and the compositions of the melts generated. We then transport the melts produced at depth to the surface to calculate the eruption rate together with the composition of the erupted lavas. Finally, we compare our numerical results to the observational data in order to constrain the melt ascent velocity.

2. Model

We follow the modeling of Jull and McKenzie (1996) with the following key differences:

- 1. While Jull and McKenzie (1996) used an ice load with a constant radius, our ice sheet behaves like a gravity current with time-dependent radius and thickness.
- 2. Our ice-load input consists of multiple deglaciation stages beginning at 23.0 to 10.5 Kyr BP designed to capture key features of ice-sheet reconstructions.
- 3. We neglect the elastic response of the solid mantle.
- 4. We assume finite melt ascent velocity.

Numerical parameters used as inputs into the model are listed in Table 1.

Numerical values of the plate half-spreading rate (U_0) , crustal thickness (z_c) , ridge angle (α) , and mantle viscosity (η) are the same as in Jull and McKenzie (1996). $z_c=20$ km is at the lower bound of the Darbyshire et al. (2000) estimates (20–37 km) because our study areas are relatively far (>100 km) from the mantle plume center. Numerical values of $U_0=10$ mm/year and $\eta=8.0\times10^{18}$ Pa s are similar to the Árnadóttir et al. (2009) estimates. The density of ice (ρ_i) is in the range of 830–917 kg/m³ in Paterson (1994). The densities of melt (ρ_1) and of solid mantle (ρ_s) follow Katz et al. (2003). Sources of the remaining numerical parameters will be mentioned later.

2.1. Glacial Load

Due to limited geological records of the ice sheet, it is not straightforward to reconstruct the details of the shape of the ice sheet during the last deglaciation (Hubbard et al., 2006; Patton et al., 2017). In Jull and

Table 1					
Parameter Values for Calculations					
Parameter	Meaning	Value	Dimensions		
D^{La}	La partition coefficient	0.010	1		
$-(\partial F/\partial P)_S$	Isentropic melt productivity	10	wt%/GPa		
g	Gravitational acceleration	9.82	m/s^2		
$P_{\rm sol}$	Solidus pressure	3.5	GPa		
U_0	Plate half-spreading rate	10	mm/year		
$z_{\rm c}$	Crustal thickness	20	km		
α	Ridge angle	45	deg		
η	Mantle viscosity	8.0×10^{18}	Pas		
$ ho_{ m i}$	Density of ice	900	kg/m ³		
$ ho_{ m l}$	Density of melt	2,900	kg/m ³		
$ ho_{ ext{S}}$	Density of solid mantle	3,300	kg/m ³		
$ au_B$	Yield stress of ice	100	kPa		

McKenzie (1996), the ice sheet was assumed to have axisymmetric parabolic shape with a constant radius of 180 km. Here we modify the ice sheet to be an axisymmetric viscous gravity current (Paterson, 1994) with glacier terminus retreating during the deglaciation. This is a more reasonable representation of the actual ice sheet, allowing the spatial variations of the volcanic response to be examined more accurately.

In an axisymmetric gravity current ice model (Huppert, 1982; Paterson, 1994), the differential thickness of ice along the radial direction induces a radially inward basal shear stress. At the yield strength limit of ice, the basal shear stress is uniform and is equal to the yield stress of ice. When the stress exceeds the yield strength limit, ice deformation and sliding will occur. These processes will readjust the ice sheet shape until it returns back to within its yield strength limit. We assume here that the time scale of the ice deformation and sliding (when the stress exceeds the yield strength) is short compared to the time scale of the deglaciation. That is, the glacier is assumed to always be within its yield strength limit and the thickness of ice h(r, t) as a function of radial distance r and time t follows (Huppert, 1982; Paterson, 1994)

$$h(r,t) = \begin{cases} h_m(t)\sqrt{1 - \frac{r}{r_m(t)}}, & 0 \le r \le r_m(t), \\ 0, & \text{otherwise,} \end{cases}$$
 (1)

where

$$h_m(t) = \left(\frac{15}{8\pi}V(t)\right)^{\frac{1}{5}} \left(\frac{2\tau_B}{\rho_1 g}\right)^{\frac{2}{5}},$$

$$r_m(t) = \left(\frac{15}{8\pi}V(t)\right)^{\frac{2}{5}} \left(\frac{\rho_1 g}{2\tau_B}\right)^{\frac{1}{5}}.$$

 $h_m(t)$ is the thickness of ice at the center, $r_m(t)$ is the radial extend of ice, V(t) is the volume of ice, ρ_i is the density of ice, and τ_B is the yield stress of ice.

The numerical value of $\tau_B = 100$ kPa we use here (Paterson, 1994) gives ice sheet dimensions that closely resemble that of the Late Weichselian Icelandic ice sheet (Hubbard et al., 2006; Licciardi et al., 2007; Patton et al., 2017; Pétursson et al., 2015; Sigmundsson, 1991) and can reproduce the ice radius of 180 km together with 2-km ice thickness used previously in Jull and McKenzie (1996).

The time evolution of the ice coverage as an input into our model follows approximately that of Patton et al. (2017). We set the input deglaciation to consist of three stages during which the ice volume decreases linearly with time and the ice volume stays constant during two intermissions between these three deglaciation stages. Time t = 0 in the model corresponds to the present (CE 1950).

We set the initial ice load to have a radius of 300 km covering the whole of Iceland and most of the continental shelf. The ice volume is held constant until t = -23.0 Kyr when the first stage of deglaciation (we refer to as the Offshore Deglaciation) begins. The Offshore Deglaciation terminates at the shoreline with ice radius

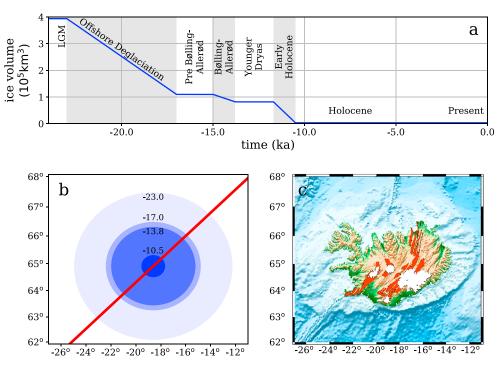


Figure 1. (a) The modeling-input ice volume history with gray bars labeling deglaciation periods. (b) Top view of the model rift (red line) with snapshots of the modeling-input ice coverage (blue circles) at time t = -23.0, -17.0, -13.8 and -10.5 Kyr as labeled at the edges of the circles. (c) Map of Iceland with the same length scale as in (b) showing locations of the fissure swarms (red color) where the plate spreading takes place and the current glaciers in white color. See Supporting Information S1 for animation of the model ice coverage map. LGM = Last Glacial Maximum.

of 180 km at time t=-17.0 Kyr followed by a pause of 2.0 Kyr. Next, the second stage of deglaciation (Bølling-Allerød) proceeds from time t=-15.0 to -13.8 Kyr during which the ice radius decreases from 180 to 160 km. Then, the deglaciation pauses for 2.1 Kyr, corresponding approximately to the Younger Dryas. The final stage of deglaciation (Early Holocene) takes place between time t=-11.7 and -10.5 Kyr with the ice sheet retreating from radius of 160 to 45 km, which is approximately the current size of the Vatnajökull ice sheet. The timeline of the modeling-input deglaciation is comparable to the last deglaciation in Iceland (Hubbard et al., 2006; Licciardi et al., 2007; Maclennan et al., 2002; Patton et al., 2017; Pétursson et al., 2015; Sigmundsson, 1991) and is summarized in Figure 1, Table 2, and Supporting Information S1.

2.2. Mantle Flow

Similar to the assumption made by Jull and McKenzie (1996), in steady state, the spreading ridge induces passive upwelling of the mantle, which we assume to follow corner flow (Batchelor, 2000; Spiegelman & McKenzie, 1987). Active upwelling induced by the mantle plume can also increase the melt production rate. However, the geological data in our study come from regions that are at least \sim 100 km away from the plume center. We therefore assume that the active upwelling is insignificant here.

Table 2 Timeline of the Model Ice Sheet						
Geological period	Time (Kyr BP)	Ice radius (km)	Average ice thickness (km)			
Last Glacial Maximum	before 23.0	300.0 constant	1.39 constant			
Offshore deglaciation	$23.0 \rightarrow 17.0$	$300.0 \rightarrow 180.0$	$1.39 \rightarrow 1.08$			
Pre-Bølling-Allerød	$17.0 \rightarrow 15.0$	180.0 constant	1.08 constant			
Bølling-Allerød	$15.0 \rightarrow 13.8$	$180.0 \rightarrow 160.0$	$1.08 \rightarrow 1.02$			
Younger Dryas	$13.8 \rightarrow 11.7$	160.0 constant	1.02 constant			
Early Holocene	$11.7 \rightarrow 10.5$	$160.0 \rightarrow 45.0$	$1.02 \rightarrow 0.54$			
Holocene	$10.5 \rightarrow \text{now}$	45.0 constant	0.54 constant			

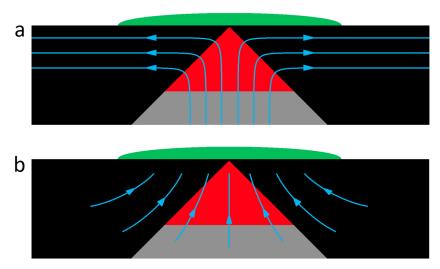


Figure 2. Simplified diagrams illustrating the solid mantle streamlines of (a) corner flow and (b) Glacial Isostatic Adjustment in a vertical plane passing through the center of ice perpendicular to the ridge axis. In steady state, the decompression melting comes from the upwelling of the mantle due to the spreading ridge (with half-spreading rate of 10 mm/year) and the mantle plume (which we assume to be insignificant in the studied areas). During deglaciation, the Glacial Isostatic Adjustment further increases the mantle upwelling rate and hence the decompression melting rate.

The glacial load on the surface affects the pressure in the mantle underneath. During deglaciation, the surface load drops, which leads to an increased mantle decompression melting rate from that induced by the steady-state passive corner flow (Figure 2).

To calculate the effect of deglaciation on mantle melting rate, we first note that the Maxwell relaxation time $(\tau_M = \eta/\mu \approx 10^1 \, {\rm years})$ is much shorter than the viscous characteristic time $(\tau_\nu = 2\eta k/\rho_{\rm s}g \approx 10^3 \, {\rm years})$ where μ is the elastic modulus, k is wave number, and other variables are as defined in Table 1. This means that the elastic deformation in the viscoelastic mantle model used in Jull and McKenzie (1996) is negligible and the deformation in the mantle is dominated by the viscous response. We therefore model the mantle as a viscous half-space incompressible fluid, and the elastic thickness of the Icelandic lithosphere is assumed to be negligible. When using the same modeling inputs as in Jull and McKenzie (1996), our numerical model yields the same results, which verifies our assumption that the elastic deformation is insignificant.

The boundary conditions on the surface of the half-space mantle are that the normal stress is equal to the pressure from the weight of the ice load and that the shear stress is negligible compared to the normal stress. We obtain semianalytical solutions to the mantle flow in cylindrical coordinates in response to the glacial load as provided in Appendix A together with the corner flow solutions.

2.3. Decompression Melting in the Mantle

Mantle upwelling is sufficiently fast that the heat loss due to conduction is negligible. Therefore, the decompression melting in the mantle is adiabatic, and the mantle melting rate DF/Dt can be calculated by (Jull & McKenzie, 1996)

$$\frac{DF}{Dt} = \left(\frac{\partial F}{\partial P}\right)_S \frac{DP}{Dt},\tag{2}$$

where F is the degree of melting by mass fraction relative to the initial mass of the solid mantle, $(\partial F/\partial P)_S$ is the isentropic melt productivity of the mantle, and $\frac{D}{Dt}$ is the convective derivative following the solid mantle trajectories.

The rate of mass production of melt per unit volume as a function of space and time is assumed to follow

$$\Gamma(\mathbf{x},t) = \rho_{s} \frac{DF}{Dt}$$

$$= \rho_{s} \left(\frac{\partial F}{\partial P}\right)_{S} \frac{DP}{Dt}.$$
(3)

The isentropic melt productivity depends on several factors including the composition of the mantle, temperature, and pressure (McKenzie, 1984). In numerical calculations, using different melt productivity functions



will result in different profiles of depth-dependent mantle melting rate and different eruptive REE concentrations (Slater et al., 1998). To investigate the effect of magma transport solely without the effect of melt productivity function on the eruptive REE concentrations, we use a constant isentropic melt productivity (Table 1), and the degree of melting as a function of pressure follows a simple linear relation

$$F(P) = -\left(\frac{\partial F}{\partial P}\right)_{S} \left(P_{\text{sol}} - P\right). \tag{4}$$

Our choice of solidus pressure and melt productivity (in Table 1) gives a melt productivity function that closely resembles that obtained from the melt parametrization of Katz et al. (2003) at 1,500 °C potential temperature.

Sims et al. (2013) have shown that the temporal variability of isotope ratios in lavas erupted during the last deglaciation in northern Iceland provide evidence for a lithologically heterogeneous mantle source beneath Iceland. We investigate the effect of mantle heterogeneities by comparing our simple homogeneous mantle model results to that of the pMELTS modeling (Ghiorso et al., 2002; Smith & Asimow, 2005) of a bilithological mantle as used in Rudge et al. (2013). We show these results in Supporting Information S1 that both mantle models yield the same conclusions for the rate of melt ascent. Our model is not very sensitive to the mantle heterogeneities because the model calculations do not involve isotopic composition.

Melts generated in the mantle have to be transported to the surface before they erupt. We assume that the effects of finite melt transport rate can be approximated by sampling the melt production rate field (equation (3)) with a time-lagged sampler. To the leading order, we assume that the vertical component of the melt velocity is constant = v_t . In this case, the time taken for melt produced at location (x, y, z) in the mantle to ascend to the surface is $\Delta t = |z|/v_t$, where |z| = -z ($\because z < 0$ below the Earth's surface). That is, melt that reaches the surface at time t is assumed to have been produced at time $t' = t - |z|/v_t$ in the past. Therefore, the total mass flux of melt supply to the crust at time t is

$$\dot{M}(t) = \int_{V} \Gamma\left(\mathbf{x}, t - \frac{|\mathbf{z}|}{v_{\star}}\right) dV, \tag{5}$$

which is the integral of all the instantaneous melts produced in the melting region \mathcal{V} ; however, the melts added from depth |z| are assumed to have been produced at time $t' = t - |z|/v_t$ in the past.

The total volume flux \dot{V} of melt supply to the crust at time t can be calculated from the mass flux:

$$\dot{V}(t) = \frac{\dot{M}(t)}{\rho_1}
= \frac{1}{\rho_1} \int_{\mathcal{V}} \Gamma\left(\mathbf{x}, t - \frac{|z|}{\nu_t}\right) dV.$$
(6)

2.4. REE Concentrations

We simplify the model by assuming that the concentration c_l^i of a highly incompatible element i with partition coefficient D^i in the instantaneous melt can be calculated based on modal fractional melting (Shaw, 1970)

$$\frac{c_1^i}{c_{s0}^i} = \frac{1}{D^i} (1 - F)^{\frac{1}{D^i} - 1},\tag{7}$$

where $c_{\rm s0}^i$ is the concentration of the element in the initial source.

Equation (7) gives the instantaneous concentration as a function of the degree of melting $c_1^i = c_1^i(F)$. The degree of melting as a function of pressure F = F(P) is known from equation (4), and the pressure as a function of position and time P = P(x, t) is known from equation (A2). We can therefore combine these equations to calculate at any location in the mantle at any time the instantaneous concentration $c_1^i = c_1^i(x, t)$ in the melt generated. The bulk partition coefficient of La (Table 1) is assumed to follow that in Workman and Hart (2005).

This very simplified melting modeling of La gives results that are not significantly different from those (shown in Supporting Information S1) obtained from a more elaborate model of mantle melting used in

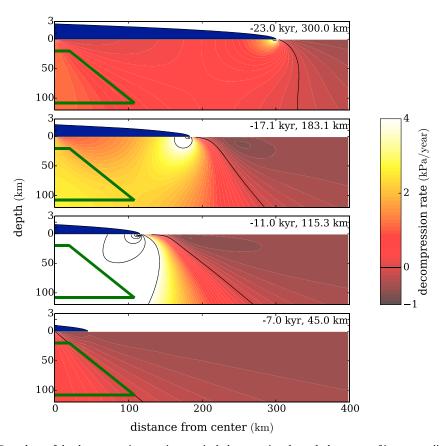


Figure 3. Snapshots of the decompression rate in a vertical plane passing through the center of ice perpendicular to the ridge axis (ridge axis as red line in Figure 1b) induced by the postglacial rebound and the corner flow. Black contour lines are separated at equal intervals of 4 kPa/year. The time and ice radius are shown in the upper right corner of each panel. The deglaciation is assumed to take place between time t = 23.0-10.5 Kyr BP with two pauses in between at t = 17.0-15.0 and 13.8-11.7 Kyr BP during which the ice volume stays constant (see section 2.1 for details). The ice-load profile (navy blue color) is drawn on top of the mantle with $15\times$ vertical exaggeration. Boundaries of the mantle melting region are outlined by the dark green lines. Animation of the decompression rates in the mantle is provided in the Supporting Information S1.

Rudge et al. (2013) because highly incompatible elements (such as La) partition into melts almost completely near the solidus intersection in the garnet field.

Given the concentration (by mass) c_1^i of a trace element i in the instantaneous melt as a function of space and time, the total mass flux of the trace element i in the melt supply to the crust is

$$\dot{M}_{i}(t) = \int_{\mathcal{V}} c_{1}^{i} \Gamma\left(\mathbf{x}, t - \frac{|\mathcal{Z}|}{\nu_{t}}\right) dV, \tag{8}$$

where c_1^i is calculated at point $(\mathbf{x}, t - \frac{|\mathbf{z}|}{v_i})$.

Similar to the volume flux of the whole melt defined in equation (6), we define the total "volume" flux of a trace element *i* in the melt supply to the crust as

$$\begin{split} \dot{V}_i(t) &= \frac{\dot{M}_i(t)}{\rho_l} \\ &= \frac{1}{\rho_l} \int_{\mathcal{V}} c_l^i \Gamma\left(\mathbf{x}, t - \frac{|\mathcal{Z}|}{\nu_t}\right) \, \mathrm{d}V. \end{split} \tag{9}$$

Following these definitions, the mean concentration of the element i in the melt supply to the crust at time t is

$$\bar{c}_{l}^{i}(t) = \frac{\dot{M}_{i}(t)}{\dot{M}(t)} = \frac{\dot{V}_{i}(t)}{\dot{V}(t)}.$$
(10)

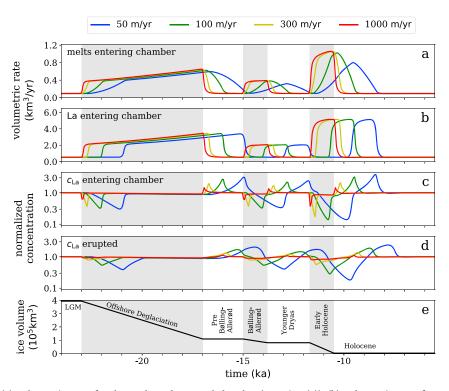


Figure 4. (a) Volumetric rate of melt supply to the crustal chamber (equation (6)). (b) Volumetric rate of La supply to the crustal chamber (equation (9)) normalized to the La concentration in the source. (c) Concentration of La in melt supply to the crustal chamber (equation (10)) normalized to the steady-state La concentration. (d) Concentration of La in erupted lavas normalized to the steady-state La concentration. (e) Modeling-input ice-load volume. (c) is the ratio of the La volume (b) to the melt volume (a); whereas (d) is the ratio of the 1,000-year SMA of the La volume (SMA of (b)) to the 1,000-year SMA of the melt volume (SMA of (a)). See section 3.5 for physical meaning of SMA used in (d). Gray shaded regions indicate the time interval during which the ice is retreating. Different line colors correspond to different values of melt ascent velocity as labeled on top of the figure in meters per year. The melt and La volumetric supply rates to the crustal chamber are the sum along the ridge axis (red line in Figure 1b) between 45 and 270 km from the center of the ice. SMA = standard moving average; LGM = Last Glacial Maximum.

3. Results and Discussion

3.1. Decompression Melting and Eruption Rates

The numerical methods we use for the calculations are discussed in Appendix B. Figure 3 illustrates snapshots of the decompression rate in the mantle from the model when the ice load history follows the timeline given in section 2.1.

While the Jull and McKenzie (1996) model with constant radius of ice load predicted that the region of maximum decompression rate is always below the center of the ice sheet (their Figure 3), our model with variable ice radius predicts that this region is below the glacier terminus and is moving radially as the ice retreats. The glacially induced decompression causes the spatially dependent mantle melting rate underneath Iceland to increase from its steady-state value by several fold during the deglaciation. These extra melts then transport to the surface, causing an increase in volcanic eruption rates.

The time delay between the surge of mantle melting and the surge of volcanic eruptions depends on the melt transport speed and also on how long melts reside in crustal chambers before they erupt. Figure 4a shows the melt supply rates to crustal chambers predicted by our model from different input values of melt ascent velocity by integrating equation (6) in the melting region underneath Iceland along the ridge axis from 45 to 270 km from the ice center, taking into account the time delay due to finite melt ascent velocity. The graph demonstrates that if melt transport was almost instantaneous, the surge in the melt supply rate (red curve) would respond almost immediately after the deglaciation period (gray shaded area). Whereas, with slower melt transport, the surge in the melt supply rate will be delayed from the deglaciation period. At lower rates of melt transport, the shape of the melt supply rate curve will be more stretched in time because melts produced at the same time at different depths will arrive at crustal chambers at different times.

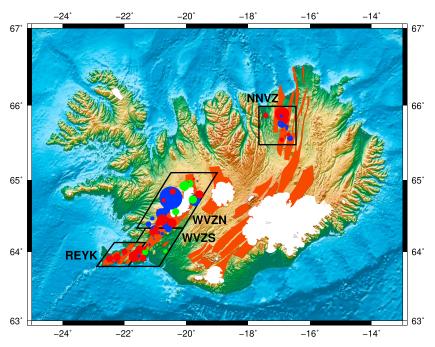


Figure 5. Mercator projection map of Iceland showing locations of eruptive units in the northern part of the Northern Volcanic Zone (NNVZ), Western Volcanic Zone-North (WVZN), Western Volcanic Zone-South (WVZS), and Reykjanes Peninsula (REYK) as circles with areas proportional to the eruptive volumes. Colors on the circles indicate the eruption types (subglacial in blue, finiglacial in green, and postglacial in red). See section 3.3 for the definition of finiglacial type. White areas show the recent Icelandic glaciers. Active fissure swarms located at where plate divergence is taking place are shown in dark red color. Data are provided in Supporting Information S1.

Note that the area under the curve over the whole time interval shown in the graph is independent of the melt ascent velocity. This is because, by the conservation of mass, the total melt supply is equal to the total melt produced regardless of how fast the melt is transported.

Before melts erupt on the surface, their compositions can be modified in the crustal chambers. We assume that the amount of melts accommodated in a chamber is constant. By conservation of mass, this implies that the total mass flux into is equal to the total mass flux out of the chamber. Therefore, the eruption rate is equal to the rate of melts entering the chamber (Figure 4a). However, the mass flux of each individual component does not need to follow this rule. Mixing and crystallization processes can modify the concentrations of REEs. We will discuss these two processes together with the remaining plots in Figure 4 later in section 3.5.

3.2. Eruptive Locations

The ages and volumes of eruptions from the last glacial and present postglacial are compiled using published maps and age estimates. The principal sources of information for the NVZ are Sæmundsson (1991) and Sæmundsson et al. (2012). For the Western Volcanic Zone (WVZ) and Reykjanes Peninsula (REYK), the maps of Sinton et al. (2005), Eason et al. (2015), and Sæmundsson et al. (2016) are used. Acknowledgements section lists all the sources of rock sample data set we use in this work.

Geological mapping, geomorphology, and interpretation of the volcanic lithologies have been used to determine the eruptive facies: whether it is subglacial, finiglacial, or postglacial. Finiglacial means that there is evidence of thin or recently disappeared ice when the eruption unit was being formed. Finiglacial units are likely to have formed when the glacier terminus was sweeping through the eruptive area during the glacial retreat.

Tephrochronology provides bounds on eruption ages for the postglacial events, meaning that the age constraints are expressed with a maximum and minimum age bound in our data set. For early postglacial and finiglacial eruptions, the maximum age has to be tied to the inferred age of deglaciation of the area, based on available reconstructions of the ice sheet history (Geirsdóttir et al., 2009; Patton et al., 2017). The ages of subglacial eruptions are, in general, not as well constrained as those of the postglacial. Minimum age constraints for these eruptions are obtained from ice-sheet reconstructions and maximum ages are set to 30 ka.



Table 3 <i>Model Distances of the Zones From Ice Center</i>				
Zone	Ranges (km)			
WVZN	0-70			
WVZS	70–180			
NNVZ	120-180			
REYK	180-250			
Note. WVZN = Western Volcanic Zone-North; WVZS = Western Volcanic Zone-South; NNVZ = Northern Volcanic Zone-North; REYK = Reykjanes Peninsula.				

Helium-3 exposure ages and the geomorphological characteristics of the uppermost surface of tuyas can also be used to infer a chronology for a subset of subglacial eruptions, using the approach of Eason et al. (2015) as informed by the data of Licciardi et al. (2007).

A table of eruptions for which age, volume, and chemical data are available is provided in Supporting Information S1. The information in this table is used to generate the plots provided for comparison with model results in this paper. The requirement of an unambiguous association between sample chemistry and eruption name, volume, and age introduces some bias into our data set: The lack of a clear link between the eruption name and chemistry means that our coverage of subglacial eruptions from the Reykjanes Peninsula is poor. Inevitably, erosion, superposition, and lack of subsurface information introduce substantial uncertainties into any reconstruction of eruptive volumes.

We divide eruption units in WVZ further into WVZ-North (WVZN) and WVZ-South (WVZS) by latitude of $64^{\circ}20'0''$. Locations and types of eruption units of all the data we use here are plotted on the map in Figure 5.

The modeling-input distances of the four zones relative to the ice center shown in Table 3 are estimates with uncertainty of almost equal to ± 50 km because the actual location of the ice center is unknown and also because of the uncertainty of the geometry of melt generation.

3.3. Eruption Types

In this section, we show how the melt ascent velocity can affect the relative volume proportion of different eruption types.

The modeling-input ice coverage radius as a function of time is known. We can therefore identify if an infinitesimal volume of melt that arrives at the surface at a particular location and time is erupted within the ice coverage radius or not. In other words, the model can divide eruptive volumes into subglacial group and subaerial group. The subglacial group corresponds approximately to the observational subglacial and finiglacial types combined. The subaerial group corresponds to the observational postglacial type. Our model does not divide the subglacial group further into subglacial and finiglacial types.

Figure 6 illustrates the model prediction that at faster melt transport (Figure 6b), there is a greater proportion of the subglacial volume (colored blue) compared to that at slower melt transport (Figure 6a). This is because faster melt transport will allow melts from depth to arrive at the surface sooner before the ice has gone. The sharp changes of subglacial to subaerial volume at 45, 160, and 180 km are due to the three pauses of the glacial terminus at these three radial distances (Table 2).

The model also predicts that for the same time interval (such as 14.5–0 Kyr BP), the relative proportion of the subglacial volume to the total volume is dependent of the distance from the ice center. This is because while most of the melts in any location are produced over the same time period during deglaciation (23.0–10.5 Kyr BP), regions closer to the ice center remain covered by ice for a longer period of time. This allows a greater proportion of melts to arrive at the surface and erupt subglacially. The spatial dependence of the subglacial to subaerial volume ratio is also seen in observations. Figure 5 illustrates that in the regions closer to the center of Iceland, there is a greater proportion of subglacial and finiglacial volumes (blue and green circles) than further out.

To compare our model results with the observations, we first note that the observational eruption volumes of units older than 14.5 Kyr BP are highly uncertain not only due to glacial erosion but also due to some older units are buried underneath younger eruptions. We therefore filter out eruptions older than 14.5 Kyr BP for

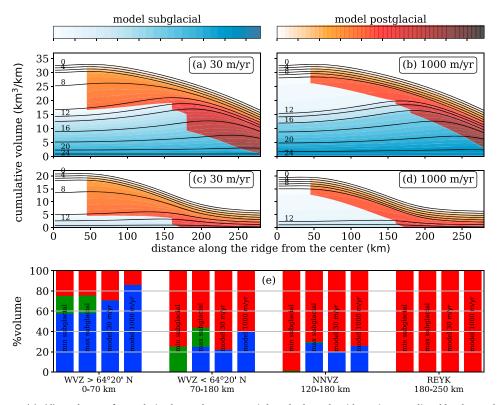


Figure 6. (a)–(d) Isochrons of cumulative lava volume per unit length along the ridge axis as predicted by the model at melt ascent velocity of 30 m/year for (a) and (c) and 1,000 m/year for (b) and (d). Subglacial and postglacial lavas are indicated by blue and red colors (as indicated by the two color bars on top of the figure) with color intensity proportional to the lava age. Contour lines are separated at an equal interval of 2 Kyr, and the ages labeled on the lines are in kiloyear before present. (a) and (b) show volume accumulated from 24.0 Kyr BP; whereas (c) and (d) show volume accumulated from 14.5 Kyr BP using the same modeling inputs as in (a) and (b). (e) Volume proportions of different eruption types that erupted between 14.5 and 0 Kyr BP in different volcanic zones. Observational data with lower and upper bounds of subglacial volumes are shown by the two left bars. The blue, green, and red bars are the subglacial, finiglacial, and postglacial volumes respectively. See section 3.3 for how the lower and upper bounds are obtained. The model results with melt ascent velocity of 30 and 1,000 m/year are shown on the two right bars with blue bars showing the subglacial and finiglacial types combined. WVZ = Western Volcanic Zone; NNVZ = Northern Volcanic Zone-North; REYK = Reykjanes Peninsula.

both the model and the observational data. The model cumulative volumes at melt ascent velocity of 30 and 1,000 m/year after the 14.5-Kyr BP filter are shown on Figures 6c and 6d. We use results from these two panels to calculate the model proportions of the subglacial volume (=observational subglacial + finiglacial) and subaerial volume (=observational postglacial) as shown on the two right bars of Figure 6e. For example, the bar plot of the model 30 m/year in NNVZ (the northern part of the Northern Volcanic Zone) on Figure 6e has subglacial (blue) and subaerial (red) proportions equal to the subglacial (blue) and subaerial (red) plotting area proportions of Figure 6c in the *x* axis range of 120–180 km.

We arrange the bar plot on Figure 6e from left to right by zone location from the closest to (WVZN) to the furthest from (REYK) the ice center. In each zone, the observational data have lower and upper estimates of subglacial volume due to age uncertainty of the subglacial units. The lower estimate (min. subglacial) shown on the left bar comes from the volume sum of the subglacial units with maximum age bound not exceeding 14.5 Kyr BP. Whereas the upper estimate (max. subglacial) comes from summing all the subglacial units with minimum age bound less than 14.5 Kyr BP (while the maximum age bound can exceed 14.5 Kyr BP).

The model predictions for spatial dependence in the diachronous response agree well with the observational data. In REYK, the whole area is already ice-free by 14.5 Kyr BP, and, hence all the eruptions are subaerial. On the other hand, WVZN remains covered by ice over most of the time during the last deglaciation, and so the majority of the eruption volumes are subglacial.

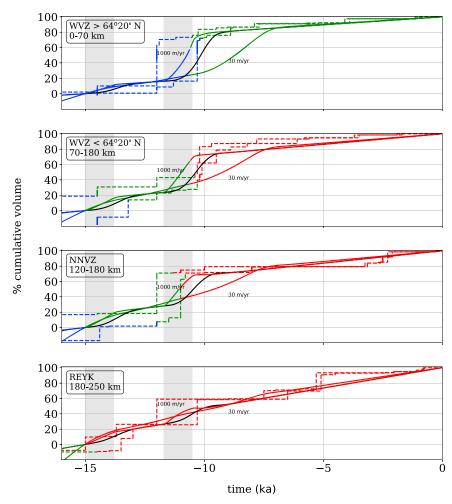


Figure 7. Cumulative eruptive volume normalized to the total volume erupted between time t=-15 and 0 Kyr. The cumulative volumes of the observational data plotted as steps (dashed lines) come from cumulating the eruptive volumes sorted by either the minimum age bounds or the maximum age bounds of the eruption units. The eruptive volume begins at 0% at -15 Kyr and ends at 100% at 0 Kyr. We use the mean cumulative volumes at these two ends to normalize the observational data. The model results for melt ascent velocity of 30 and 1,000 m/year are plotted as nonblack colored solid lines. Colors on these dashed and solid lines illustrate the eruption periods: subglacial in blue, transitional in green, and postglacial in red (see section 3.4 for definition of the transitional period). Black solid line in each panel shows the model result for melt ascent velocity of 100 m/year. The timings of the eruption periods for the black curve are the same as those for the remaining model-result curves. Different panels correspond to different volcanic zones as indicated on the upper-left corner of each panel together with the corresponding modeling-input zone range (section 3.2). Gray shaded regions indicate the time interval during which the modeling-input ice is retreating. WVZ = Western Volcanic Zone; NNVZ = Northern Volcanic Zone-North; REYK = Reykjanes Peninsula.

Results on Figure 6e also suggest that the melt ascent velocity is likely to be of the order of 100 m/year. At below 30 m/year, the subglacial volumes predicted by the model would be smaller than that of the observational lower bound estimates (min. subglacial). Nevertheless, we note that the model results depend on the distance along the ridge axis over which the melts are integrated (as estimated in section 3.2). Similar to the model, the observational lava volumes in the four zones are also integrated over ridge lengths of \sim 60–90 km.

3.4. Timing of the Peaks in Volcanic Productivity

Another way to estimate the melt ascent velocity is to use the timing of the peaks in volcanic productivity. On Figure 7, we plot the cumulative eruptive volume as a function of time for the model outputs and the observational data. This figure shows that the bursts in the cumulative lava volume predicted by the model at melt ascent velocities between 30 and 1,000 m/year have timings approximately equal to that of the observations across all the volcanic zones to within the uncertainties of the lava ages and the modeling-input ice load history.



In the period during which the glacier terminus was sweeping through each zone (called transitional period), some areas in the zone are already ice-free, while some areas are still covered by ice. This means that, in the transitional period, eruptions can be either subglacial or subaerial.

In the observational data sorted by age, the transitional period can be identified approximately by the period during which there are some alternations of the timeline orders between subglacial, finiglacial, and postglacial types. The remaining two end periods are called subglacial and postglacial periods. The subglacial period consists of only subglacial type, and the postglacial period consists of only postglacial type. In the model, the transitional period is identified by the period during which the ice radius is in the zone range (as listed in Table 3).

The timing of the periods in the model is controlled by the input ice history and the input zone range. Therefore, a well-matched timing of the periods between the model and the observational data helps us identify if the modeling inputs of ice load and zone range reasonably reflect the actual values. The discrepancy between the observations and the model results at our preferred estimate of 100 m/year melt ascent velocity is likely to be because of the uncertainty of the observational eruption ages and the model axisymmetric ice assumption.

Nevertheless, the results in Figure 7 show that, at a melt ascent velocity of 30 m/year or below, the difference of the timing in the burst in volcanism between the model results and the observational data becomes significant. More quantitatively, with the average mantle melting depth of ≈ 50 km, reducing the melt ascent velocity from 100 to 30 m/year will delay the burst timing by ≈ 1.2 Kyr, which is significant compared to the uncertainty of the eruption ages. Our model implies a similar lower bound value to that of 50 m/year estimated in Maclennan et al. (2002) from the relative timing between the observed eruption ages and the deglaciation. An advantage of this work is that much broader geographical spread is accounted for. Our model examines eruptions in different volcanic zones; whereas Maclennan et al. (2002) only examined eruptions in the NNVZ region.

3.5. Geochemical Response

3.5.1. Model Predictions

Figure 4b shows the volumetric supply rate of La to the crustal chambers normalized to the steady-state La concentration. Similarly to the whole melts in Figure 4a, the surge in the supply rate of La is delayed from the deglaciation period due to the finite speed of melt transport. However, while the volumetric melt supply rate curves (Figure 4a) are stretched in time, the La supply rate curves (Figure 4b) retain their shapes almost like the same time series but time shifted. This is because La is partitioned into melt at almost the same depth (near the solidus). Most of the La takes almost an equal time to arrive at the crust regardless of how fast the ascent rate is. Therefore, changing the ascent rate will not significantly spread the La flux out along the time axis. In contrast, melts are produced at different depths. They take different times to transport to the crust. The slower the ascent rate, the more the time delay between melts from different depths to arrive at the surface; hence, the more the spread of the melt supply rate curve along the time axis.

Figure 4c is the La concentration (c_{La}) in the melt supply to the crustal chambers, which is equal to Figure 4b divided by Figure 4a. This would correspond to the concentration in the lava erupted at the surface if the magma mixing process in the crustal chamber was not present. The longer the magma is allowed to mix in the crustal chamber, the smaller the variation signal of the REE concentrations.

In the model, the effect of magma mixing on $c_{\rm La}$ in the lavas is equivalent mathematically to the time average concentration. The time period over which the average is performed is equal to the time duration that the magmas mix in the crustal chamber before they erupt. In a study of the chemical disequilibria between olivine, its melt inclusions, and the whole melts that surround the olivine in rock samples collected from Iceland, Maclennan (2008) estimated that the magma residence time is of the order of a few hundreds to \lesssim 1,000 years. We therefore take the time average $c_{\rm La}$ over a period of 1,000 years, and the result is shown in Figure 4d. In other words, this panel is equal to the ratio between the 1,000-year standard moving average (SMA) of La volume supply to the crustal chamber (1,000-year SMA of Figure 4b) and the 1,000-year SMA of the whole melt volume supply to the crustal chamber (1,000-year SMA of Figure 4a).

Note that melt mixing also occurs "en route," while melts are migrating from depths to the crustal chamber and meet together along the way. This geological process corresponds mathematically to the volume integration over the mantle melting domain \mathcal{V} as shown in equation (9), taking into account the time delay due



to the finite rate of melt transport Δt . In other words, the model results shown in Figures 4b–4d as calculated by equations (9) and (10) have already taken into account the effect of en route melt mixing.

Our results in Figures 4c and 4d show that the variation of $c_{\rm La}$ is strongly dependent on the melt ascent velocity. The lower the melt ascent velocity, the higher the variation of $c_{\rm La}$. This effect can be explained as follows. During the deglaciation, the decompression rate in the mantle is maximum at the surface and decays exponentially with depth (as illustrated in Figure 3). This means that the extra melts generated during deglaciation are mostly produced at shallow depths in the mantle, which is depleted in La. If the melt transport had been instantaneous, the extra melts produced at any depth at the same time would have traveled to the crust and mixed instantly and would have erupted at the surface with La depletion of up to $\approx\!20\%$ as predicted by Jull and McKenzie (1996). In contrast, when the melt ascent velocity is finite, the extra melts produced at shallower depths during deglaciation will arrive at the surface before the extra melts produced at deeper depths. The slower the rate of melt transport, the more likely the extra melts from shallow depths (La depleted) are to erupt before they mix with the extra melts from deep depths (La enriched). As a result, when the melt ascent velocity is sufficiently low, the first arrival of the extra melts produced during deglaciation will be much more depleted in La than that predicted by the instantaneous melt transport model of Jull and McKenzie (1996).

The eruptive $c_{\rm La}$ will recover back to near the steady-state concentration after the extra melts from the bottom of the melting region (La enriched) catch up and mix with the extra melts from shallow depths (La depleted) before they erupt. Moreover, the recovery of the eruptive $c_{\rm La}$ back to the steady-state will overshoot after the deglaciation ends. This phenomenon can be explained as follows. Once the deglaciation terminates, the glacially induced decompression melting in the mantle will also terminate at all depths at the same time, and the extra melt supply to the surface from shallow depths (La depleted) will run out before the extra melt supply from deep depths (La enriched). This is because the melts from greater depths take a longer time to arrive at the surface. Therefore, once the La depleted melt supply from the shallow depths runs out, the remaining majority of the erupted lavas will be the La-enriched melts from deep depths, and the eruption will become enriched in La.

Figure 4d also shows that the timing of the periods during which the lavas are enriched or depleted in La is dependent on the melt ascent velocity. At slower melt ascent velocity, the peaks and the troughs of $c_{\rm La}$ are delayed further from the deglaciation periods. Hence, we can use this timing combined with the magnitude of the $c_{\rm La}$ variations to estimate the melt ascent velocity. We note that the La-depleted lava volume dominates the La-enriched lava volume. This can be seen in Figure 4. The troughs of $c_{\rm La}$ (Figure 4d) fall in the periods of the bursts in eruption rates (Figure 4a); whereas the peaks of $c_{\rm La}$ (Figure 4d) fall outside those periods. Therefore, the La-depletion signal is stronger than the La-enrichment signal, which is also seen in observational data. The majority of the eruptions during the last deglaciation are depleted in La. **3.5.2. Geological Observations**

The eruptive La concentrations of observational data are from rock samples collected from Iceland by the previous studies (see Acknowledgements section and Supporting Information S1 for details). These rock samples are of melts that have gone through fractionation/accumulation during cooling and crystallization processes in the crustal chambers. These processes modify the melt compositions from their original precrustal compositions.

We make fractionation/accumulation correction of $c_{\rm La}$ in each rock sample based on the MgO content of the sample. We assume that the precrustal melts have 14.0 wt% MgO as estimated in Maclennan et al. (2001). Rock samples that have MgO between 9.5 and 14.0 wt% are assumed to have undergone crystallization of olivine-rich material with 40.0 wt% MgO. If the melts underwent crystallization further below 9.5 wt% MgO, they generate a gabbroic solid with 11.0 wt% MgO. Some rock samples have higher MgO content than 14.0 wt% of the precrustal melts. We assume that these samples are from melts that have been influenced by the accumulation of olivine crystals with 40.0 wt% MgO.

Due to the age uncertainty of eruption units, $c_{\rm La}$ cannot be plotted directly as that of the model in Figure 4. Most of the eruptions have their age estimated as a time band bounded by some geological events with identifiable age (e.g., tephra layers). In WVZ and NNVZ, most of the eruption units fall into one of the following age bands:

- 1. Glacial (pre-14.5/14.4 Kyr BP)
- 2. Eruptive Pulse 1 (14.5/14.4 to 12.0 Kyr BP)

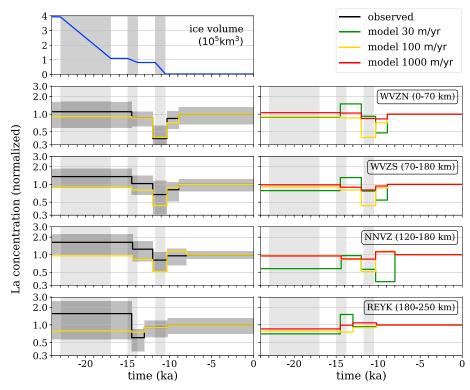


Figure 8. Top panel is the modeling-input ice volume. Each row of the remaining panels shows La concentrations normalized to the steady-state concentration in each volcanic zone. The upper-right corner of the right panel labels the corresponding zone and the modeling-input zone range. On the left panel, the black curve shows the observational La concentrations together with gray bands indicating ± 1 standard deviation of rock samples. The yellow curve is the model result from a melt ascent velocity of 100 m/year. The right panel illustrates the model La concentrations calculated from different values of melt ascent velocity labeled with different line colors. Details of how the La concentrations are calculated can be found in the text. WVZN = Western Volcanic Zone-North; WVZS = Western Volcanic Zone-South; NNVZ = Northern Volcanic Zone-North; REYK = Reykjanes Peninsula.

- 3. Eruptive Pulse 2 (12.0 to 10.3 Kyr BP)
- 4. Early Postglacial (10.3 to 8.9/8.0 Kyr BP)
- 5. Steady-State Postglacial (post-8.9/8.0 Kyr BP)

REYK zone is different in that it is the furthest from the ice center and became ice-free by 14.5 Kyr BP, which is earlier than the other zones. Eruption units in REYK are divided into the following age bands:

- 1. Glacial (pre-14.5 Kyr BP)
- 2. Early Postglacial 1 (14.5 to 13.0 Kyr BP)
- 3. Early Postglacial 2 (13.0 to 10.2 Kyr BP)
- 4. Steady-State Postglacial (post-10.2 Kyr BP)

In each of these age bands, we take the volume-weighted average La concentration normalized to the Steady-State Postglacial La concentration and plot in Figure 8 for both the observational data and the model.

The right column of Figure 8 illustrates that different model melt ascent velocities result in different La concentration characteristics. In each age band, some values of melt ascent velocity may predict La depletion, whereas the others predict La enrichment. This is due to the effect of melt ascent velocity on the timing of the peaks and troughs of $c_{\rm La}$ (Figure 4d) that we discussed earlier.

The left column of Figure 8 shows that the model melt ascent velocity of 100 m/year yields similar $c_{\rm La}$ characteristics to that of the observations. At two extreme melt ascent velocities of 30 and 1,000 m/year, the $c_{\rm La}$ characteristics are significantly different from that of the observations both in the timing and the magnitude of the $c_{\rm La}$ variations.



In the Glacial age band, the observational $c_{\rm La}$ is elevated from the Steady-State Postglacial value in all the volcanic zones. This is likely to be due to the effect of glacial loading on depth-dependent melting suppression that occurred before the Last Glacial Maximum (23 Kyr BP). This feature is not included in our model here, which may explain why the model $c_{\rm La}$ in the Glacial age band is lower than that observed across all the volcanic zones. One of our future works will be to investigate this glacial loading effect.

3.6. Model Limitations

The accuracy of our results depends on several factors. The deviations of modeling input parameters from the actual geological values that are not well-constrained can be significant.

For example, the model La concentration is dependent on the time period over which the magma mixes in the crustal chamber. As mentioned in section 3.5, the longer the magma residence time, the lower the variations of La concentrations. Also, the residence time may not be the same throughout Iceland as assumed in our model. A better constraint on the effective magma residence time in the chamber may therefore be required.

Our 100-m/year estimate of the melt ascent velocity likely represents that of the melt produced during the glacially induced isostatic adjustment (GIA). At steady state, the decompression melting rate is significantly less. This leads to a significantly lower mass flux of melt and likely results in a slower rate of melt transport. This could be one reason why our ascent rate estimate is significantly higher than that in models of melt transport at Mid-Ocean Ridges (Burley & Katz, 2015; Crowley et al., 2015). A melt ascent velocity of 100 m/year is $\sim 2 \text{ orders}$ of magnitude faster than would be predicted from simple models of diffuse porous flow. As has been noted in several previous studies, such rapid melt ascent velocities suggest that some focusing or channelization of melt must occur during transport (e.g., Kelemen et al., 1997).

In more elaborate fluid dynamic models (e.g., McKenzie, 1984), the melt velocity varies with depth. Melt flow starts slow at the base of the melting region and ascends at a faster rate as it migrates to a shallower depth where the porosity is higher. Therefore, in any region below the GIA average melting depth, the melt ascent velocity is likely to be below our estimate. This depth-dependent melt ascent velocity would cause a more time delay of the burst of the La supply rate to the crustal chamber than that predicted by our model in Figure 4b. A larger time delay between the melt supply and the La supply would increase the time intervals during which the La concentration (Figures 4c and 4d) is depleted or enriched.

2-D fluid dynamic models of melt and trace element transport (e.g., Spiegelman, 1996) also predict an across-axis variation in the erupted melt composition. In our model, we assume complete melt mixing and extraction on the ridge axis. This produces only a single average concentration of La at each snapshot in time. Spiegelman (1996) also showed that the convergence of melt to the ridge axis in passive ridge flow leads to an enrichment of incompatible elements in the erupted melt by almost a factor of 2 (for $D^i \leq 0.01$) from that in the 1-D column model. If the full solution of melt transport had been incorporated into our model, the La concentration at steady state would have also been increased by a factor of \sim 2. If the same enrichment factor (\sim 2) also uniformly applies to that during the GIA, our model results of the La concentration (normalized to the steady-state value) would remain unchanged. However, the flow fields of the solid mantle and of the melts during the GIA are certainly different from those at steady state. Therefore, the enrichment factor during the GIA is unlikely to be uniformly the same as that at the steady state. How much the enrichment factor varies still remains to be explored. In our future work, we would like to incorporate full melt transport solutions into the model to understand how good the constant ascent rate approximation is.

The real ice-sheet shape may be significantly deviated from the axisymmetric shape that we use. While our axisymmetric assumption helps simplify the computations, a modeling-input ice sheet with more detailed 3-D shape may have an important role in controlling the accuracy of the model results.

Last but not least, the time evolution of the ice sheet shape we input into our model may be significantly different from the actual ice sheet. For example, the glacier may extensively readvance in some periods during the last deglaciation. Glacial advance will increase the load on the surface, which will lead to pressure increase in the mantle. This will suppress mantle melting and can also affect the REE concentrations as discussed in section 3.5. The modeling of the effects of glacial advance on mantle melting beneath Iceland may therefore be important.



4. Conclusions

The consequences of a finite melt ascent velocity on lavas erupted during the last deglaciation are the following:

- 1. Volume proportions of different eruption types: Faster melt transport will allow more melts to arrive at the surface and erupt sooner when the ice is still present. This means that there will be a greater proportion of subglacial and finiglacial volumes relative to postglacial volume.
- 2. Relative timing between the bursts in the eruption rates and the deglaciation: Higher melt ascent velocity will transport the extra melts produced during deglaciation to the surface faster. This will result in a smaller time lag between the bursts in the eruption rates and the deglaciation.
- 3. Variations of REE concentrations: Slower melt ascent velocity will result in a greater time lag between melts from shallow depth (REE depleted) and melts from deep depth (REE enriched) arriving at the surface. This will cause higher variations of REE concentrations in the lavas.

Our numerical model estimates that the Icelandic melt transport from the upper mantle melting region to the surface during the last deglaciation has an average melt ascent velocity of the order of \sim 100 m/year.

Appendix A: Mantle Flow

In steady state, the velocity components of the mantle flow follow the corner flow solutions. In Cartesian coordinates, they can be written as (Batchelor, 2000; Spiegelman & McKenzie, 1987)

$$v_x(x, y, z) = \frac{Bxz}{x^2 + z^2} - B \arctan \left(\frac{x}{z}\right),$$

$$v_y(x, y, z) = 0,$$
and
$$v_z(x, y, z) = \frac{Bz^2}{x^2 + z^2} - B \sin^2(\alpha),$$
(A1)

where

$$B = \frac{2U_0}{\pi - 2\alpha - \sin(2\alpha)},$$

 v_x is the horizontal velocity component perpendicular to the ridge, v_y is the horizontal velocity component parallel to the ridge, v_z is the velocity component in the vertical direction, U_0 is the half-spreading velocity of the ridge, and α is the ridge angle from the horizontal.

Ice-load change causes GIA. In cylindrical coordinates, the semianalytical solutions to the axisymmetric GIA response in the viscous half-space mantle are

$$\begin{split} v_r(r,z,t) &= -\frac{\rho_{\rm i}}{\rho_{\rm s}} \mathcal{H}_1^{-1} \left[kz e^{kz} \tilde{w}(k,t) \right], \\ v_\theta(r,z,t) &= 0, \\ v_z(r,z,t) &= -\frac{\rho_{\rm i}}{\rho_{\rm s}} \mathcal{H}_0^{-1} \left[(1-kz) e^{kz} \tilde{w}(k,t) \right], \\ P(r,z,t) &= -\rho_{\rm s} gz + \rho_{\rm i} g \mathcal{H}_0^{-1} \left[\tau e^{kz} \tilde{w}(k,t) \right], \\ \text{and} \qquad &\frac{DP}{Dt} (r,z,t) = \rho_{\rm i} g \mathcal{H}_0^{-1} \left[e^{kz} \left(\mathcal{H}_0[\dot{h}](k,t) - kz \tilde{w}(k,t) \right) \right], \end{split}$$

where

$$\tau \equiv \tau(k) = \frac{2\eta k}{\rho_s g},$$

$$\tilde{w}(k,t) = \int_{t_{\rm iso}}^{t} \left(\mathcal{H}_0[\dot{h}](k,t') \right) \exp \left(-\frac{t-t'}{\tau} \right) \mathrm{d}t' / \tau,$$

$$\mathcal{H}_n[f](k) = \int_0^{\infty} f(r) J_n(kr) r \mathrm{d}r,$$

$$\mathcal{H}_n^{-1}[F](r) = \int_0^{\infty} F(k) J_n(kr) k \, \mathrm{d}k,$$



 v_r is the radial component of the velocity, v_θ is the azimuthal component of the velocity, v_z is the vertical component of the velocity, P is the pressure in the mantle, ρ_i is the density of ice, ρ_s is the density of the mantle, \dot{h} is the time derivative of the thickness of ice sheet, $\mathcal{H}_n[f]$ is the nth-order Hankel transform of function f, $\mathcal{H}_n^{-1}[F]$ is the nth-order inverse Hankel transform of function F, I_n is the nth-order Bessel function of the first kind, and I_n is the wave number. I_n in the I_n in the I_n is the time at which the mantle is in isostatic equilibrium.

Equation (A2) shows that the glacially induced decompression rate depends on the history of the deglaciation rate \dot{h} and is attenuated exponentially with depth by the e^{kz} factor (z < 0 in the mantle). For the ice-sheet shape in equation (1), the Hankel transform of the rate of change of ice load is analytical:

$$\mathcal{H}_{0}[\dot{h}](k,t) = \frac{3\sqrt{2}}{32}\dot{V}(t)\left[J_{-\frac{1}{4}}\left(\frac{kr_{m}(t)}{2}\right)J_{\frac{1}{4}}\left(\frac{kr_{m}(t)}{2}\right) + J_{-\frac{3}{4}}\left(\frac{kr_{m}(t)}{2}\right)J_{\frac{3}{4}}\left(\frac{kr_{m}(t)}{2}\right)\right]. \tag{A3}$$

Appendix B: Numerical Methods

Calculations of the melting rates, the eruption rates, and the REE concentrations (equations (5), (6), (8), and (9)) require temporal and spatial integrations over a finite domain. We perform these numerical integrations using the trapezoidal rule. We discretize the spatial domain using a 3-D rectangular grid with uniform horizontal and vertical resolutions of 5-by-5 km² and 0.5 km, respectively.

For an REE with $D^i \ll 1$, the concentration c_1^i changes rapidly with depth near the solidus. As can be seen in equation (7), c_1^i drops sharply with F near the solidus F=0. By adopting the trapezoidal rule to integrate equation (8) along the depth using values of c_1^i at the grid vertices alone, the trapezoidal error can be very significant. In order to resolve this rapid change within each cell of the grid, we calculate c_1^i inside the cell using equation (7) with F=F(z) that is obtained from linear interpolation of the face-averaged F between the lower face and upper face of the cell with depth z. The face-averaged value of a face is simply the mean value of the four vertices at the corners of the face. This technique helps improve the model c_1^i accuracy significantly.

Calculations of mantle flow and decompression rates such as equation (A2) involve the inverse Hankel transform, which requires numerical integration of the wave number k from 0 to ∞ . All the mathematical expressions in the model that require inverse Hankel transform contain an attenuation factor e^{kz} , which decays exponentially with the wave number k in the mantle (z < 0). Therefore, the numerical integration of the inverse Hankel transform from k = 0 to ∞ can be truncated when the attenuation factor e^{kz} is negligibly small. In our model, the melting region is at z = -20 km or below. We truncate the integration at k = 2/3 km⁻¹, which corresponds to $e^{kz} \sim 2 \times 10^{-6}$ or below.

The variations of integrands of all the inverse Hankel transform involved in the model are dominated by the ice-load function in the k domain (equation (A3)). This function consists of the nth-order Bessel functions of the first kind J_n with $n=\pm 1/4$ and $\pm 3/4$, all of which have the same argument $=kr_m/2$ where r_m is the ice radius. This means that the ice-load function in the k domain varies with k at a frequency of $\sim r_m/2 \sim 100$ km. We therefore use the trapezoidal strip size dk=1/1,440 km⁻¹, which gives $dkr_m/2 \leq 10^{-1}$. This corresponds to having at least $N_k=10$ trapezoidal strips per unit length in the nondimensional k domain since $N_k=2/(dkr_m)\geq 10$.



The decompression rate = -DP/Dt at time t can be calculated directly from equation (A2) independently from any information in the previous time steps. This means that the time step size does not affect the accuracy of the model. We use a uniform time step size of 50 years.

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